



Fig. 5/50 SIPROTEC 7SJ63 multifunction protection relay

Description

The SIPROTEC 7SJ63 can be used as a protective control and monitoring relay for distribution feeders and transmission lines of any voltage in networks that are earthed (grounded), low-resistance grounded, ungrounded, or of a compensated neutral point structure. The relay is suited for networks that are radial or looped, and for lines with single or multi-terminal feeds. Regarding the time-overcurrent/directional overcurrent protection the characteristics can be either definite time, inverse time or user-defined.

The SIPROTEC 7SJ63 is equipped with motor protection applicable for asynchronous machines of all sizes. Motor protection comprises undercurrent monitoring, starting time supervision, restart inhibit, locked rotor.

The relay provides easy-to-use local control and automation functions. The number of controllable switchgear depends only on the number of available inputs and outputs. The integrated programmable logic (CFC) allows the user to implement their own functions, e.g. for the automation of switchgear (interlocking). The user is able to generate user-defined messages as well.

Function overview

Protection functions

- Overcurrent protection (definite-time/inverse-time/user-def.)
- Directional overcurrent protection (definite-time/inverse-time/user-def.)
- Sensitive dir./non-dir. ground-fault detection
- Displacement voltage
- Intermittent ground-fault protection
- High-impedance restricted ground fault
- Inrush restraint
- Motor protection
- Overload protection
- Temperature monitoring
- Under-/overvoltage protection
- Under-/overfrequency protection
- Breaker failure protection
- Negative-sequence protection
- Phase-sequence monitoring
- Auto-reclosure
- Fault locator
- Lockout

Control functions/programmable logic

- Flexible number of switching devices
- Position of switching elements is shown on the graphic display
- Local/remote switching via key-operated switch
- Control via keyboard, binary inputs, DIGSI 4 or SCADA system
- Extended user-defined logic with CFC (e.g. interlocking)

Monitoring functions

- Operational measured values V, I, f, \dots
- Energy metering values W_p, W_q
- Circuit-breaker wear monitoring
- Slave pointer
- Trip circuit supervision
- Fuse failure monitor
- 8 oscillographic fault records

Communication interfaces

- System interface
 - IEC 60870-5-103, IEC 61850
 - PROFIBUS DP
 - DNP 3 / MODBUS RTU
- Service interface for DIGSI 4 (modem)
- Front interface for DIGSI 4
- Time synchronization via IRIG-B/DCF77

Overcurrent Protection / 7SJ63

Application

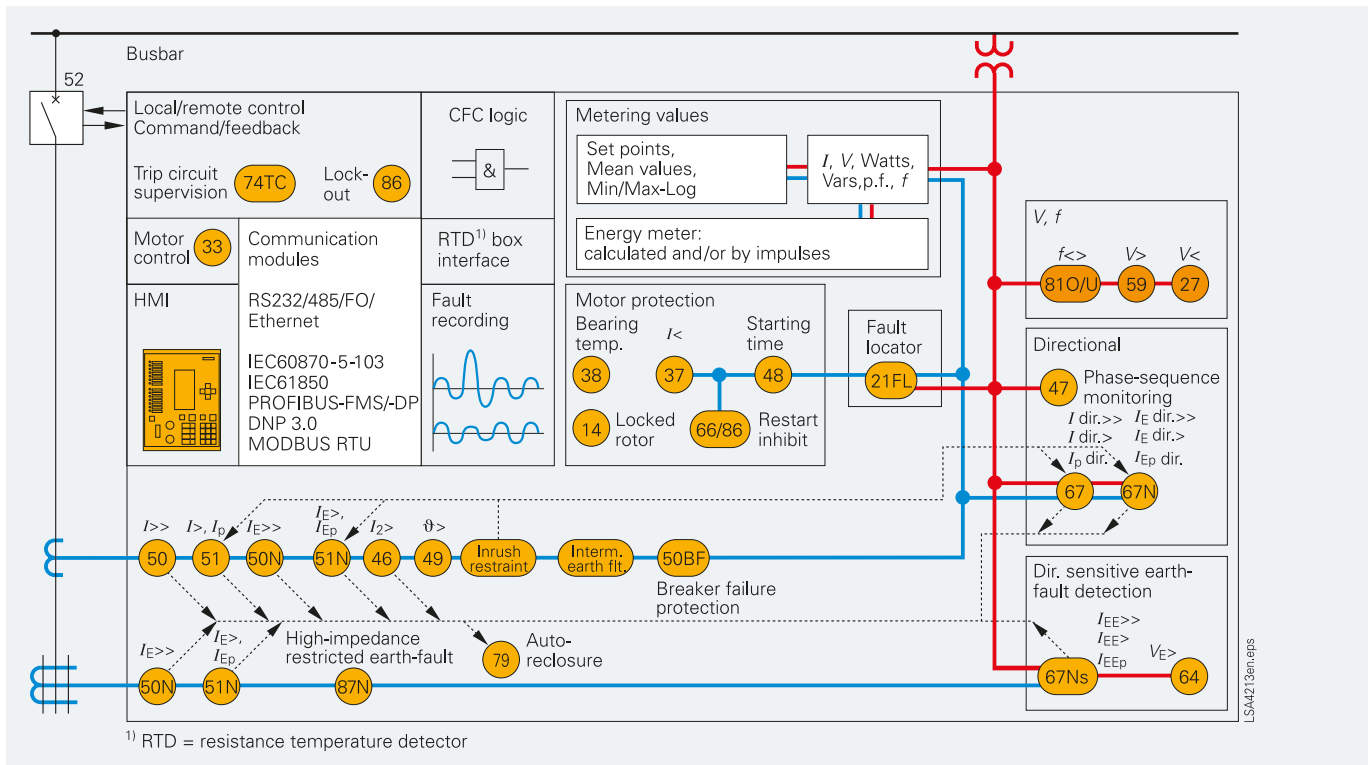


Fig. 5/51 Function diagram

Application

The SIPROTEC 7SJ63 unit is a numerical protection relay that also performs control and monitoring functions and therefore supports the user in cost-effective power system management, and ensures reliable supply of electric power to the customers. Local operation has been designed according to ergonomic criteria. A large, easy-to-read graphic display was a major design aim.

Control

The integrated control function permits control of disconnect devices (electrically operated/motorized switches) or circuit-breakers via the integrated operator panel, binary inputs, DIGSI 4 or the control and protection system (e.g. SICAM). The present status (or position) of the primary equipment can be displayed. 7SJ63 supports substations with single and duplicate busbars. The number of elements that can be controlled (usually 1 to 5) is only restricted by the number of inputs and outputs available. A full range of command processing functions is provided.

Programmable logic

The integrated logic characteristics (CFC) allow the user to implement their own functions for automation of switchgear (interlocking) or a substation via a graphic user interface. The user can also generate user-defined messages.

Line protection

The 7SJ63 units can be used for line protection of high and medium-voltage networks with earthed (grounded), low-resistance grounded, isolated or compensated neutral point.

Motor protection

When protecting motors, the 7SJ63 relays are suitable for asynchronous machines of all sizes.

Transformer protection

The 7SJ63 units perform all functions of backup protection supplementary to transformer differential protection. The inrush suppression effectively prevents tripping by inrush currents.

The high-impedance restricted ground-fault protection detects short-circuits and insulation faults on the transformer.

Backup protection

The relays can be used universally for backup protection.

Metering values

Extensive measured values, limit values and metering values permit improved systems management.

ANSI	IEC	Protection functions
50, 50N	$I>$, $I>>$ $I_E>$, $I_E>>$	Definite-time overcurrent protection (phase/neutral)
50, 51V, 51N	I_p , I_{Ep}	Inverse overcurrent protection (phase/neutral), phase function with voltage-dependent option
67, 67N	$I_{dir}>$, $I_{dir}>>$, $I_{p\ dir}$ $I_{Edir}>$, $I_{Edir}>>$, $I_{p\ dir}$	Directional overcurrent protection (definite/inverse, phase/neutral), Directional comparison protection
67Ns/50Ns	$I_{EE}>$, $I_{EE}>>$, I_{EEp}	Directional/non-directional sensitive ground-fault detection
-		Cold load pick-up (dynamic setting change)
59N/64	V_E , $V_0>$	Displacement voltage, zero-sequence voltage
-	$I_{IE}>$	Intermittent ground fault
87N		High-impedance restricted ground-fault protection
50BF		Breaker failure protection
79		Auto-reclosure
46	$I_2>$	Phase-balance current protection (negative-sequence protection)
47	$V_2>$, phase seq.	Unbalance-voltage protection and/or phase-sequence monitoring
49	$\vartheta>$	Thermal overload protection
48		Starting time supervision
14		Locked rotor protection
66/86		Restart inhibit
37	$I<$	Undercurrent monitoring
38		Temperature monitoring via external device (RTD-box), e.g. bearing temperature monitoring
27, 59	$V<$, $V>$	Undervoltage/overvoltage protection
81O/U	$f>$, $f<$	Overfrequency/underfrequency protection
21FL		Fault locator

Overcurrent Protection / 7SJ63

Construction

Construction

Connection techniques and housing with many advantages

½ and ¼-rack sizes

These are the available housing widths of the 7SJ63 relays, referred to a 19" module frame system. This means that previous models can always be replaced. The height is a uniform 244 mm for flush-mounting housings and 266 mm for surface-mounting housings for all housing widths. All cables can be connected with or without ring lugs. Plug-in terminals are available as an option.

It is thus possible to employ prefabricated cable harnesses. In the case of surface mounting on a panel, the connection terminals are located above and below in the form of screw-type terminals. The communication interfaces are located in a sloped case at the top and bottom of the housing. The housing can also be supplied optionally with a detached operator panel (refer to Fig. 5/54), or without operator panel, in order to allow optimum operation for all types of applications.

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Fig. 5/52 Flush-mounting housing with screw-type terminals

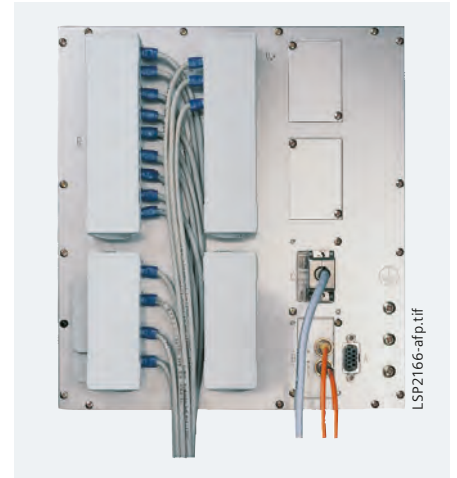


Fig. 5/53 Rear view of flush-mounting housing with covered connection terminals and wirings



Fig. 5/54 Housing with plug-in terminals and detached operator panel



Fig. 5/55 Surface-mounting housing with screw-type terminals

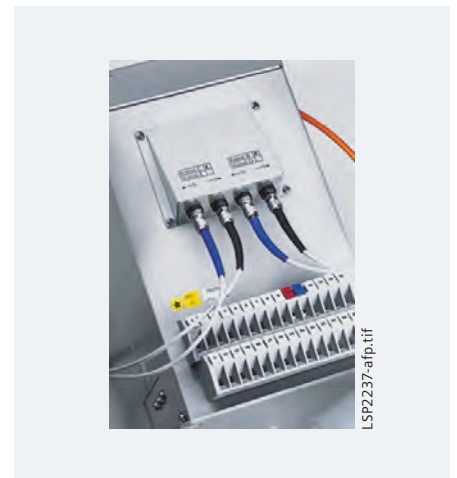


Fig. 5/56 Communication interfaces in a sloped case in a surface-mounting housing

Protection functions

Overcurrent protection (ANSI 50, 50N, 51, 51N)

This function is based on the phase-selective measurement of the three phase currents and the ground current (four transformers). Two definite-time overcurrent protection elements (DMT) exist both for the phases and for the ground. The current threshold and the delay time can be set within a wide range. In addition, inverse-time overcurrent protection characteristics (IDMTL) can be activated.

Reset characteristics

For easier time coordination with electro-mechanical relays, reset characteristics according to ANSI C37.112 and IEC 60255-3/BS 142 standards are applied.

When using the reset characteristic (disk emulation), a reset process is initiated after the fault current has disappeared. This reset process corresponds to the reverse movement of the Ferraris disk of an electromechanical relay (thus: disk emulation).

User-definable characteristics

Instead of the predefined time characteristics according to ANSI, tripping characteristics can be defined by the user for phase and ground units separately. Up to 20 current/time value pairs may be programmed. They are set as pairs of numbers or graphically in DIGSI 4.

Inrush restraint

The relay features second harmonic restraint. If the second harmonic is detected during transformer energization, pickup of non-directional and directional normal elements are blocked.

Cold load pickup/dynamic setting change

For directional and non-directional overcurrent protection functions the initiation thresholds and tripping times can be switched via binary inputs or by time control.

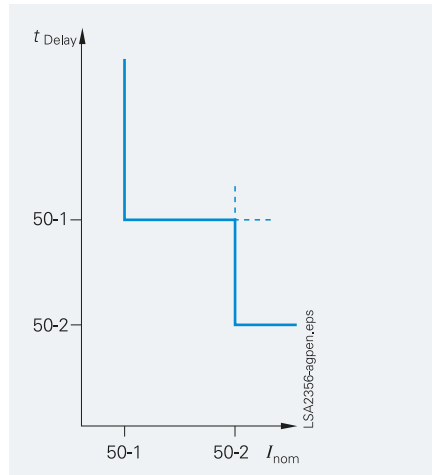


Fig. 5/57 Definite-time overcurrent protection

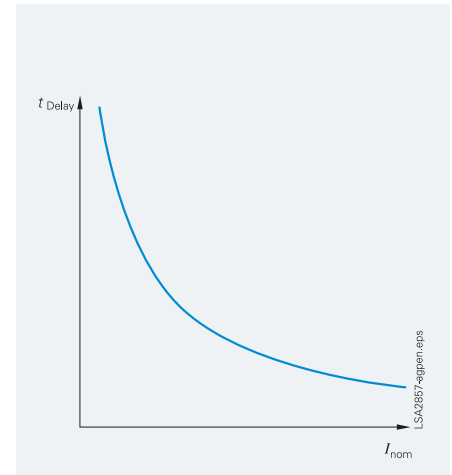


Fig. 5/58 Inverse-time overcurrent protection

Available inverse-time characteristics		
Characteristics acc. to	ANSI/IEEE	IEC 60255-3
Inverse	•	•
Short inverse	•	
Long inverse	•	•
Moderately inverse	•	
Very inverse	•	•
Extremely inverse	•	•

Overcurrent Protection / 7SJ63

Protection functions

Directional overcurrent protection (ANSI 67, 67N)

Directional phase and ground protection are separate functions. They operate in parallel to the non-directional overcurrent elements. Their pickup values and delay times can be set separately. Definite-time and inverse-time characteristic is offered. The tripping characteristic can be rotated about ± 180 degrees.

By means of voltage memory, directionality can be determined reliably even for close-in (local) faults. If the switching device closes onto a fault and the voltage is too low to determine direction, directionality (directional decision) is made with voltage from the voltage memory. If no voltage exists in the memory, tripping occurs according to the coordination schedule.

For ground protection, users can choose whether the direction is to be determined via zero-sequence system or negative-sequence system quantities (selectable). Using negative-sequence variables can be advantageous in cases where the zero voltage tends to be very low due to unfavorable zero-sequence impedances.

Directional comparison protection (cross-coupling)

It is used for selective protection of sections fed from two sources with instantaneous tripping, i.e. without the disadvantage of time coordination. The directional comparison protection is suitable if the distances between the protection stations are not significant and pilot wires are available for signal transmission. In addition to the directional comparison protection, the directional coordinated overcurrent protection is used for complete selective backup protection. If operated in a closed-circuit connection, an interruption of the transmission line is detected.

(Sensitive) directional ground-fault detection (ANSI 64, 67Ns, 67N)

For isolated-neutral and compensated networks, the direction of power flow in the zero sequence is calculated from the zero-sequence current I_0 and zero-sequence voltage V_0 . For networks with an isolated neutral, the reactive current component is evaluated; for compensated networks, the active current component or residual resistive current is evaluated. For special network conditions, e.g. high-resistance grounded networks with ohmic-capacitive ground-fault current or low-resistance grounded networks with ohmic-inductive current, the tripping characteristics can be rotated approximately ± 45 degrees.

Two modes of ground-fault direction detection can be implemented: tripping or "signalling only mode".

It has the following functions:

- TRIP via the displacement voltage V_E .
- Two instantaneous elements or one instantaneous plus one user-defined characteristic.
- Each element can be set in forward, reverse, or non-directional.
- The function can also be operated in the insensitive mode as an additional short-circuit protection.

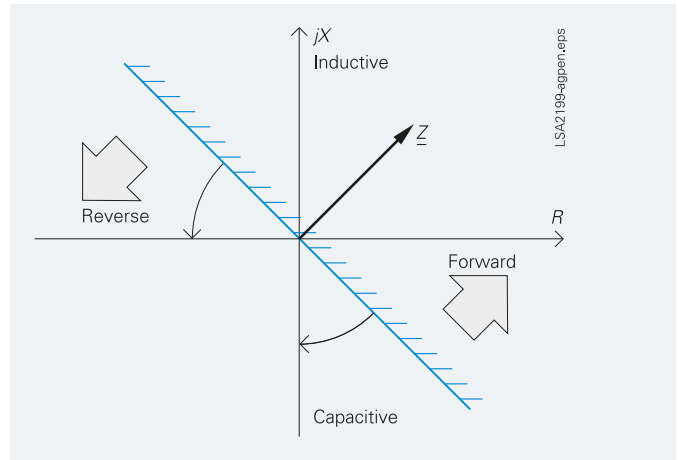


Fig. 5/59 Directional characteristic of the directional overcurrent protection

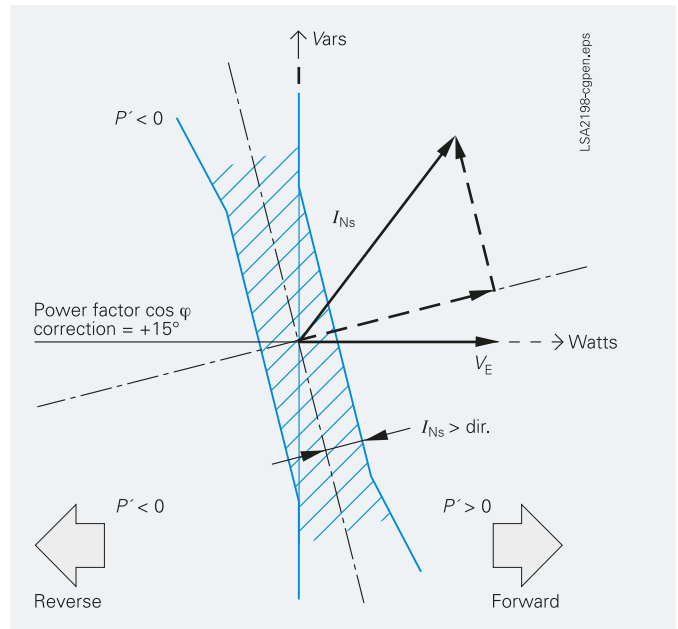


Fig. 5/60 Directional determination using cosine measurements for compensated networks

(Sensitive) ground-fault detection (ANSI 50Ns, 51Ns / 50N, 51N)

For high-resistance grounded networks, a sensitive input transformer is connected to a phase-balance neutral current transformer (also called core-balance CT).

The function can also be operated in the insensitive mode as an additional short-circuit protection.

Intermittent ground-fault protection

Intermittent (re-striking) faults occur due to insulation weaknesses in cables or as a result of water penetrating cable joints. Such faults either simply cease at some stage or develop into lasting short-circuits. During intermittent activity, however, star-point resistors in networks that are impedance-grounded may undergo thermal overloading. The normal ground-fault pro-

tection cannot reliably detect and interrupt the current pulses, some of which can be very brief.

The selectivity required with intermittent ground faults is achieved by summing the duration of the individual pulses and by triggering when a (settable) summed time is reached. The response threshold I_{IE} evaluates the r.m.s. value, referred to one systems period.

Phase-balance current protection (ANSI 46) (Negative-sequence protection)

In line protection, the two-element phase-balance current/negative-sequence protection permits detection on the high side of high-resistance phase-to-phase faults and phase-to-ground faults that are on the low side of a transformer (e.g. with the switch group Dy 5). This provides backup protection for high-resistance faults beyond the transformer.

Breaker failure protection (ANSI 50BF)

If a faulted portion of the electrical circuit is not disconnected upon issuance of a trip command, another command can be initiated using the breaker failure protection which operates the circuit-breaker, e.g. of an upstream (higher-level) protection relay. Breaker failure is detected if, after a trip command, current is still flowing in the faulted circuit. As an option, it is possible to make use of the circuit-breaker position indication.

High-impedance restricted ground-fault protection (ANSI 87N)

The high-impedance measurement principle is an uncomplicated and sensitive method for detecting ground faults, especially on transformers. It can also be applied to motors, generators and reactors when these are operated on an grounded network.

When the high-impedance measurement principle is applied, all current transformers in the protected area are connected in parallel and operated on one common resistor of relatively high R whose voltage is measured (see Fig. 5/61). In the case of 7SJ6 units, the voltage is measured by detecting the current through the (external) resistor R at the sensitive current measurement input I_{EE} . The varistor V serves to limit the voltage in the event of an internal fault. It cuts off the high momentary voltage spikes occurring at transformer saturation. At the same time, this results in smoothing of the voltage without any noteworthy reduction of the average value.

If no faults have occurred and in the event of external faults, the system is at equilibrium, and the voltage through the resistor is approximately zero. In the event of internal faults, an imbalance occurs which leads to a voltage and a current flow through the resistor R .

The current transformers must be of the same type and must at least offer a separate core for the high-impedance restricted ground-fault protection. They must in particular have the same transformation ratio and an approximately identical knee-point voltage. They should also demonstrate only minimal measuring errors.

Auto-reclosure (ANSI 79)

Multiple reclosures can be defined by the user and lockout will occur if a fault is present after the last reclosure. The following functions are possible:

- 3-pole ARC for all types of faults
- Separate settings for phase and ground faults

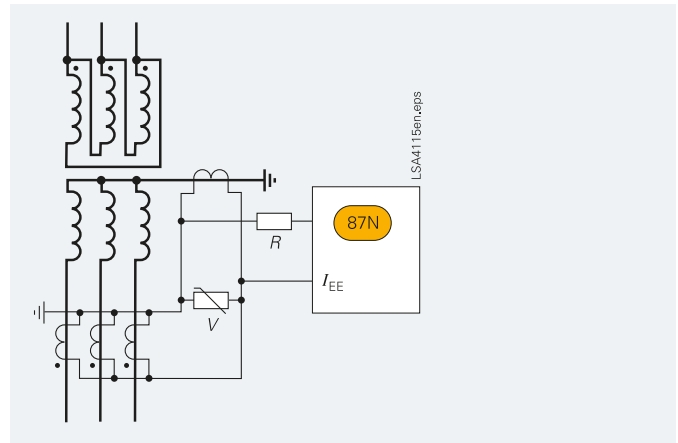


Fig. 5/61 High-impedance restricted ground-fault protection

- Multiple ARC, one rapid auto-reclosure (RAR) and up to nine delayed auto-reclosures (DAR)
- Starting of the ARC depends on the trip command selection (e.g. 46, 50, 51, 67)
- Blocking option of the ARC via binary inputs
- ARC can be initiated externally or via CFC
- The directional and non-directional elements can either be blocked or operated non-delayed depending on the auto-reclosure cycle
- Dynamic setting change of the directional and non-directional elements can be activated depending on the ready AR

Thermal overload protection (ANSI 49)

For protecting cables and transformers, an overload protection with an integrated pre-warning element for temperature and current can be applied. The temperature is calculated using a thermal homogeneous-body model (according to IEC 60255-8), which takes account both of the energy entering the equipment and the energy losses. The calculated temperature is constantly adjusted accordingly. Thus, account is taken of the previous load and the load fluctuations.

For thermal protection of motors (especially the stator) a further time constant can be set so that the thermal ratios can be detected correctly while the motor is rotating and when it is stopped. The ambient temperature or the temperature of the coolant can be detected serially via an external temperature monitoring box (resistance-temperature detector box, also called RTD-box). The thermal replica of the overload function is automatically adapted to the ambient conditions. If there is no RTD-box it is assumed that the ambient temperatures are constant.

Settable dropout delay times

If the devices are used in parallel with electromechanical relays in networks with intermittent faults, the long dropout times of the electromechanical devices (several hundred milliseconds) can lead to problems in terms of time grading. Clean time grading is only possible if the dropout time is approximately the same. This is why the parameter of dropout times can be defined for certain functions such as time-overcurrent protection, ground short-circuit and phase-balance current protection.

Protection functions

■ Motor protection

Restart inhibit (ANSI 66/86)

If a motor is started up too many times in succession, the rotor can be subject to thermal overload, especially the upper edges of the bars. The rotor temperature is calculated from the stator current. The reclosing lockout only permits start-up of the motor if the rotor has sufficient thermal reserves for a complete start-up (see Fig. 5/62).

Emergency start-up

This function disables the reclosing lockout via a binary input by storing the state of the thermal replica as long as the binary input is active. It is also possible to reset the thermal replica to zero.

Temperature monitoring (ANSI 38)

Up to two temperature monitoring boxes with a total of 12 measuring sensors can be used for temperature monitoring and detection by the protection relay. The thermal status of motors, generators and transformers can be monitored with this device.

Additionally, the temperature of the bearings of rotating machines are monitored for limit value violation. The temperatures are being measured with the help of temperature detectors at various locations of the device to be protected. This data is transmitted to the protection relay via one or two temperature monitoring boxes (see "Accessories", page 5/153).

Starting time supervision (ANSI 48/14)

Starting time supervision protects the motor against long unwanted start-ups that might occur in the event of excessive load torque or excessive voltage drops within the motor, or if the rotor is locked. Rotor temperature is calculated from measured stator current. The tripping time is calculated according to the following equation:

for $I > I_{\text{MOTOR START}}$

$$t = \left(\frac{I_A}{I} \right)^2 \cdot T_A$$

- I = Actual current flowing
- $I_{\text{MOTOR START}}$ = Pickup current to detect a motor start
- t = Tripping time
- I_A = Rated motor starting current
- T_A = Tripping time at rated motor starting current

If the trip time is rated according to the above formula, even a prolonged start-up and reduced voltage (and reduced start-up current) will be evaluated correctly. The tripping time is inverse (current dependent).

A binary signal is set by a speed sensor to detect a blocked rotor. An instantaneous tripping is effected.

Phase-balance current protection (ANSI 46) (Negative-sequence protection)

The negative-sequence / phase-balance current protection detects a phase failure or load unbalance due to network asymmetry and protects the rotor from impermissible temperature rise.

Undercurrent monitoring (ANSI 37)

With this function, a sudden drop in current, which can occur due to a reduced motor load, is detected. This may be due to shaft breakage, no-load operation of pumps or fan failure.

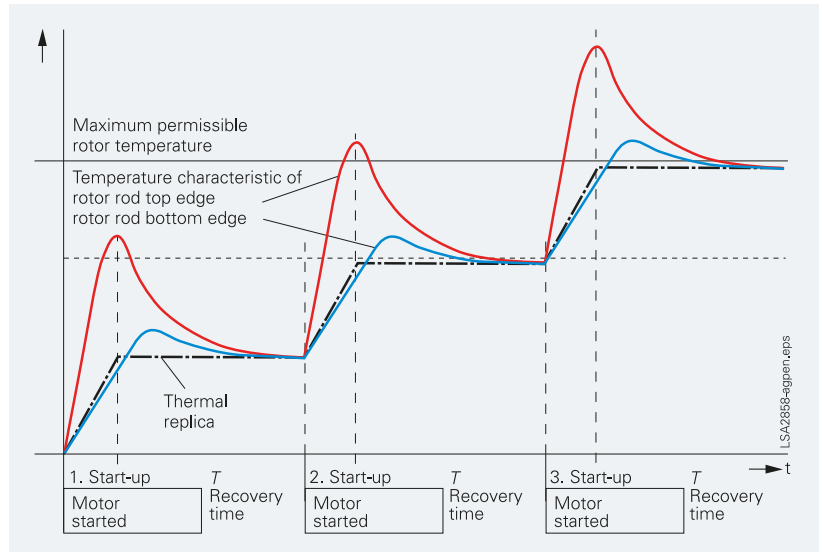


Fig. 5/62

■ Voltage protection

Overvoltage protection (ANSI 59)

The two-element overvoltage protection detects unwanted network and machine overvoltage conditions. The function can operate either with phase-to-phase voltage (default) or with the negative phase-sequence system voltage. Three-phase and single-phase connections are possible.

Undervoltage protection (ANSI 27)

The two-element undervoltage protection provides protection against dangerous voltage drops (especially for electric machines). Applications include the isolation of generators or motors from the network to avoid undesired operating states and a possible loss of stability. Proper operating conditions of electrical machines are best evaluated with the positive-sequence quantities. The protection function is active over a wide frequency range (45 to 55, 55 to 65 Hz)¹⁾. Even when falling below this frequency range the function continues to work, however, with a greater tolerance band.

The function can operate either with the positive phase-sequence system voltage (default) or with the phase-to-phase voltages, and can be monitored with a current criterion. Three-phase and single-phase connections are possible.

Frequency protection (ANSI 81O/U)

Frequency protection can be used for over-frequency and under-frequency protection. Electric machines and parts of the system are protected from unwanted speed deviations. Unwanted frequency changes in the network can be detected and the load can be removed at a specified frequency setting. Frequency protection can be used over a wide frequency range (45 to 55, 55 to 65 Hz)¹⁾. There are four elements (selectable as overfrequency or underfrequency) and each element can be delayed separately. Blocking of the frequency protection can be performed if using a binary input or by using an undervoltage element.

Fault locator (ANSI 21FL)

The fault locator specifies the distance to a fault location in kilometers or miles or the reactance of a second fault operation.

1) The 45 to 55, 55 to 65 Hz range is available for $f_N = 50/60$ Hz.

Circuit-breaker wear monitoring

Methods for determining circuit-breaker contact wear or the remaining service life of a circuit-breaker (CB) allow CB maintenance intervals to be aligned to their actual degree of wear. The benefit lies in reduced maintenance costs.

There is no mathematically exact method of calculating the wear or the remaining service life of circuit-breakers that takes into account the arc-chamber's physical conditions when the CB opens. This is why various methods of determining CB wear have evolved which reflect the different operator philosophies. To do justice to these, the devices offer several methods:

- ΣI
- ΣI^x , with $x = 1 \dots 3$

The devices additionally offer a new method for determining the remaining service life:

- Two-point method

The CB manufacturers double-logarithmic switching cycle diagram (see Fig. 5/63) and the breaking current at the time of contact opening serve as the basis for this method. After CB opening, the two-point method calculates the number of still possible switching cycles. To this end, the two points P1 and P2 only have to be set on the device. These are specified in the CB's technical data.

All of these methods are phase-selective and a limit value can be set in order to obtain an alarm if the actual value falls below or exceeds the limit value during determination of the remaining service life.

Customized functions (ANSI 32, 51V, 55, etc.)

Additional functions, which are not time critical, can be implemented via the CFC using measured values. Typical functions include reverse power, voltage controlled overcurrent, phase angle detection, and zero-sequence voltage detection.

Commissioning

Commissioning could hardly be easier and is fully supported by DIGSI 4. The status of the binary inputs can be read individually and the state of the binary outputs can be set individually. The operation of switching elements (circuit-breakers, disconnect devices) can be checked using the switching functions of the bay controller. The analog measured values are represented as wide-ranging operational measured values. To prevent transmission of information to the control center during maintenance, the bay controller communications can be disabled to prevent unnecessary data from being transmitted. During commissioning, all indications with test marking for test purposes can be connected to a control and protection system.

Test operation

During commissioning, all indications can be passed to an automatic control system for test purposes.

■ Control and automatic functions

Control

In addition to the protection functions, the SIPROTEC 4 units also support all control and monitoring functions that are required for operating medium-voltage or high-voltage substations.

The main application is reliable control of switching and other processes.

The status of primary equipment or auxiliary devices can be obtained from auxiliary contacts and communicated to the 7SJ63 via binary inputs. Therefore it is possible to detect and indicate both the OPEN and CLOSED position or a fault or intermediate circuit-breaker or auxiliary contact position.

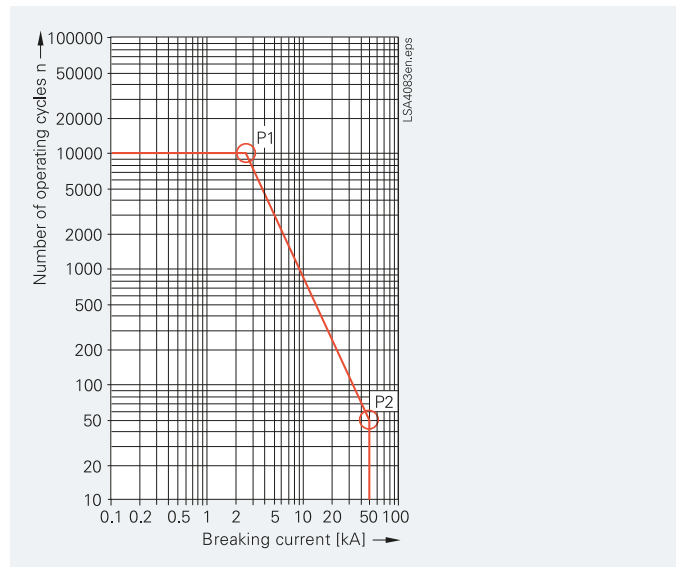


Fig. 5/63 CB switching cycle diagram

The switchgear or circuit-breaker can be controlled via:

- integrated operator panel
- binary inputs
- substation control and protection system
- DIGSI 4

Automation / user-defined logic

With integrated logic, the user can set, via a graphic interface (CFC), specific functions for the automation of switchgear or substation. Functions are activated via function keys, binary input or via communication interface.

Switching authority

Switching authority is determined according to parameters, communication or by key-operated switch (when available). If a source is set to "LOCAL", only local switching operations are possible. The following sequence of switching authority is laid down: "LOCAL"; DIGSI PC program, "REMOTE".

Key-operated switch

7SJ63 units are fitted with key-operated switch function for local/remote changeover and changeover between interlocked switching and test operation.

Command processing

All the functionality of command processing is offered. This includes the processing of single and double commands with or without feedback, sophisticated monitoring of the control hardware and software, checking of the external process, control actions using functions such as runtime monitoring and automatic command termination after output. Here are some typical applications:

- Single and double commands using 1, 1 plus 1 common or 2 trip contacts
- User-definable bay interlocks
- Operating sequences combining several switching operations such as control of circuit-breakers, disconnectors and grounding switches
- Triggering of switching operations, indications or alarm by combination with existing information

Overcurrent Protection / 7SJ63

Functions

Functions

Motor control

The SIPROTEC 7SJ63 with high performance relays is well-suited for direct activation of the circuit-breaker, disconnector and grounding switch operating mechanisms in automated substations.

Interlocking of the individual switching devices takes place with the aid of programmable logic. Additional auxiliary relays can be eliminated. This results in less wiring and engineering effort.

Assignment of feedback to command

The positions of the circuit-breaker or switching devices and transformer taps are acquired by feedback. These indication inputs are logically assigned to the corresponding command outputs. The unit can therefore distinguish whether the indication change is a consequence of switching operation or whether it is a spontaneous change of state.

Chatter disable

Chatter disable feature evaluates whether, in a configured period of time, the number of status changes of indication input exceeds a specified figure. If exceeded, the indication input is blocked for a certain period, so that the event list will not record excessive operations.

Indication filtering and delay

Binary indications can be filtered or delayed.

Filtering serves to suppress brief changes in potential at the indication input. The indication is passed on only if the indication voltage is still present after a set period of time. In the event of indication delay, there is a wait for a preset time. The information is passed on only if the indication voltage is still present after this time.

Indication derivation

A further indication (or a command) can be derived from an existing indication. Group indications can also be formed. The volume of information to the system interface can thus be reduced and restricted to the most important signals.

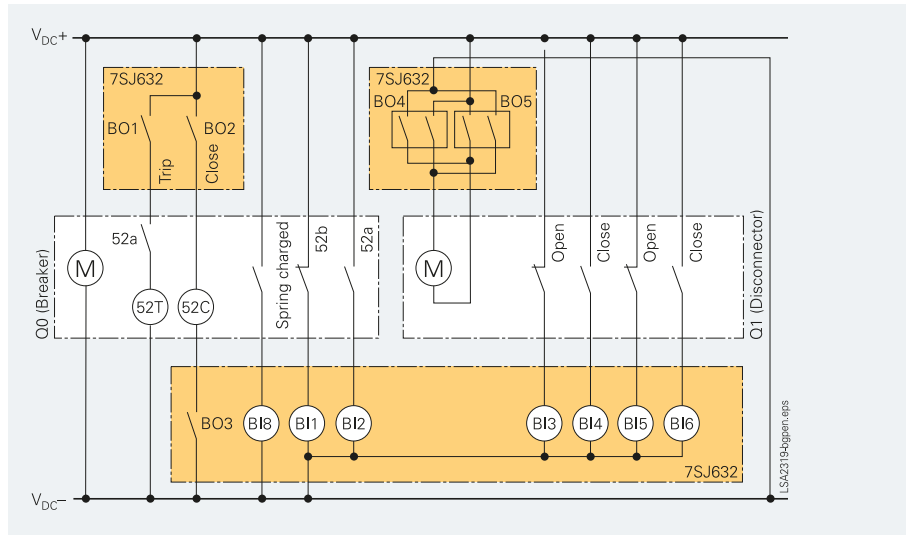


Fig. 5/64 Typical wiring for 7SJ632 motor direct control (simplified representation without fuses). Binary output BO4 and BO5 are interlocked so that only one set of contacts are closed at a time.

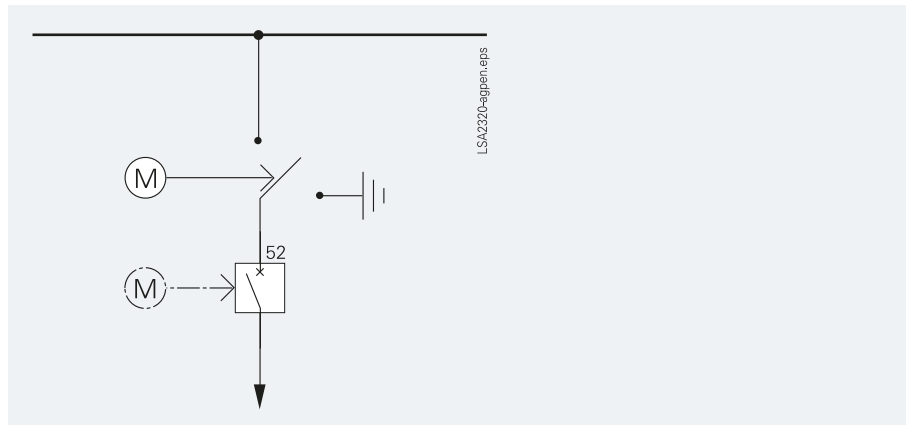


Fig. 5/65 Example: Single busbar with circuit-breaker and motor-controlled three-position switch

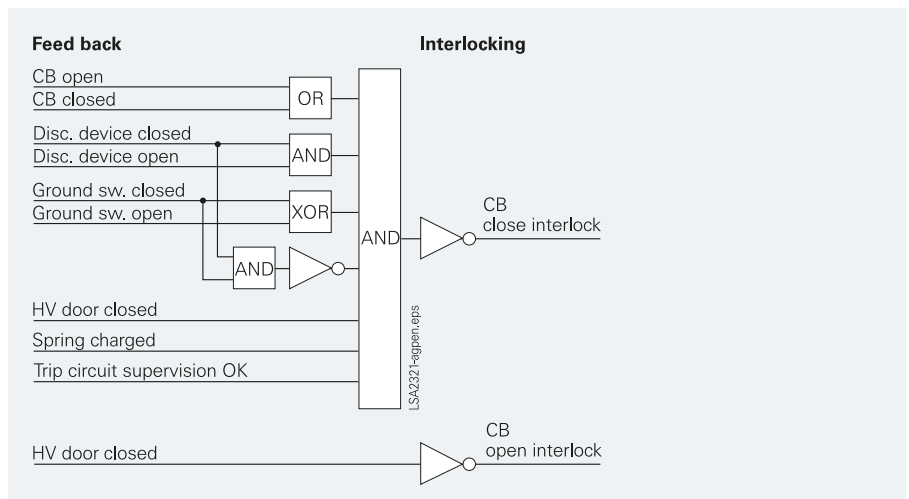


Fig. 5/66 Example: Circuit-breaker interlocking

Measured values

The r.m.s. values are calculated from the acquired current and voltage along with the power factor, frequency, active and reactive power. The following functions are available for measured value processing:

- Currents I_{L1} , I_{L2} , I_{L3} , I_E , I_{EE} (67Ns)
- Voltages V_{L1} , V_{L2} , V_{L3} , V_{L1L2} , V_{L2L3} , V_{L3L1}
- Symmetrical components I_1 , I_2 , $3I_0$; V_1 , V_2 , V_0
- Power Watts, Vars, VA/P, Q , S (P , Q : total and phase selective)
- Power factor ($\cos \varphi$), (total and phase selective)
- Frequency
- Energy \pm kWh, \pm kVarh, forward and reverse power flow
- Mean as well as minimum and maximum current and voltage values
- Operating hours counter
- Mean operating temperature of overload function
- Limit value monitoring
Limit values are monitored using programmable logic in the CFC. Commands can be derived from this limit value indication.
- Zero suppression
In a certain range of very low measured values, the value is set to zero to suppress interference.

Metered values

For internal metering, the unit can calculate an energy metered value from the measured current and voltage values. If an external meter with a metering pulse output is available, the SIPROTEC 4 unit can obtain and process metering pulses via an indication input.

The metered values can be displayed and passed on to a control center as an accumulation with reset. A distinction is made between forward, reverse, active and reactive energy.



Fig. 5/67 NX PLUS panel (gas-insulated)

Measuring transducers

- Characteristic with knee
For measuring transducers it sometimes makes sense to extend a small range of the input value, e.g. for the frequency that is only relevant in the range 45 to 55, 55 to 65 Hz. This can be achieved by using a knee characteristic.
- Live-zero monitoring
4 – 20 mA circuits are monitored for open-circuit detection.

Switchgear cubicles for high/medium voltage

All units are designed specifically to meet the requirements of high/medium-voltage applications.

In general, no separate measuring instruments (e.g. for current, voltage, frequency measuring transducer ...) or additional control components are necessary.

Overcurrent Protection / 7SJ63

Communication

Communication

In terms of communication, the units offer substantial flexibility in the context of connection to industrial and power automation standards. Communication can be extended or added on thanks to modules for retrofitting on which the common protocols run. Therefore, also in the future it will be possible to optimally integrate units into the changing communication infrastructure, for example in Ethernet networks (which will also be used increasingly in the power supply sector in the years to come).

Serial front interface

There is a serial RS232 interface on the front of all the units. All of the unit's functions can be set on a PC by means of the DIGSI 4 protection operation program. Commissioning tools and fault analysis are also built into the program and are available through this interface.

Rear-mounted interfaces¹⁾

A number of communication modules suitable for various applications can be fitted in the rear of the flush-mounting housing. In the flush-mounting housing, the modules can be easily replaced by the user.

The interface modules support the following applications:

- Time synchronization interface
All units feature a permanently integrated electrical time synchronization interface. It can be used to feed timing telegrams in IRIG-B or DCF77 format into the units via time synchronization receivers.
- System interface
Communication with a central control system takes place through this interface. Radial or ring type station bus topologies can be configured depending on the chosen interface. Furthermore, the units can exchange data through this interface via Ethernet and IEC 61850 protocol and can also be operated by DIGSI.
- Service interface
The service interface was conceived for remote access to a number of protection units via DIGSI. On all units, it can be an electrical RS232/RS485 or an optical interface. For special applications, a maximum of two temperature monitoring boxes (RTD-box) can be connected to this interface as an alternative.

System interface protocols (retrofittable)

IEC 61850 protocol

The Ethernet-based IEC 61850 protocol is the worldwide standard for protection and control systems used by power supply corporations. Siemens was the first manufacturer to support this standard. By means of this protocol, information can also be exchanged directly between bay units so as to set up simple masterless systems for bay and system interlocking. Access to the units via the Ethernet bus is also possible with DIGSI.

IEC 60870-5-103 protocol

The IEC 60870-5-103 protocol is an international standard for the transmission of protective data and fault recordings. All messages from the unit and also control commands can be transferred by means of published, Siemens-specific extensions to the protocol.

1) For units in panel surface-mounting housings please refer to note on page 5/130.

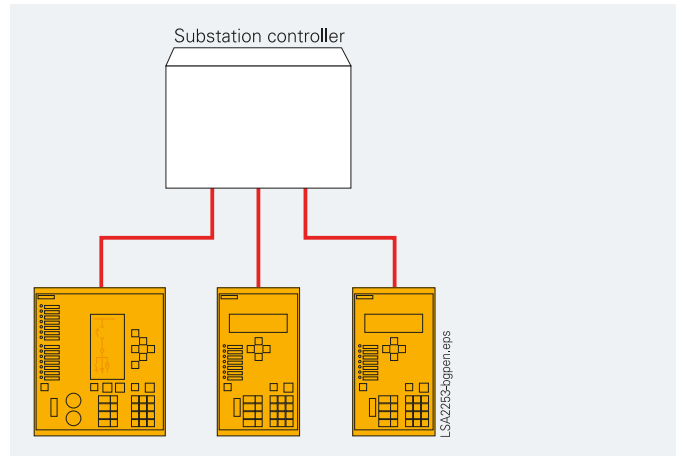


Fig. 5/68 IEC 60870-5-103: Radial fiber-optic connection

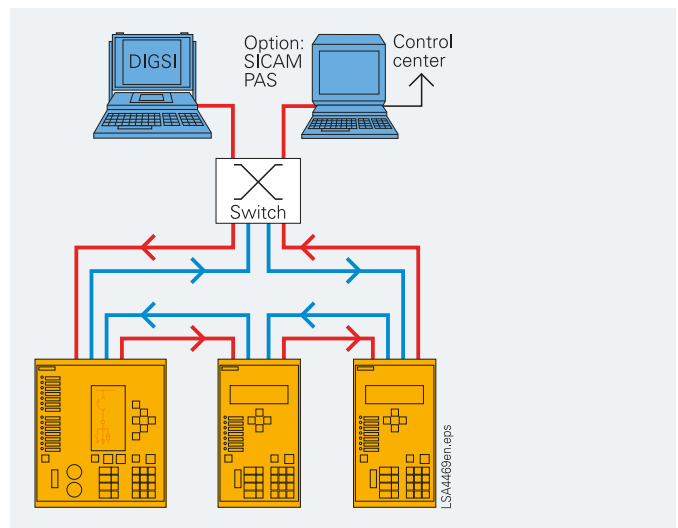


Fig. 5/69 Bus structure for station bus with Ethernet and IEC 61850, fiber-optic ring

PROFIBUS DP protocol

PROFIBUS DP is the most widespread protocol in industrial automation. Via PROFIBUS DP, SIPROTEC units make their information available to a SIMATIC controller or, in the control direction, receive commands from a central SIMATIC. Measured values can also be transferred.

MODBUS RTU protocol

This uncomplicated, serial protocol is mainly used in industry and by power supply corporations, and is supported by a number of unit manufacturers. SIPROTEC units function as MODBUS slaves, making their information available to a master or receiving information from it. A time-stamped event list is available.

DNP 3.0 protocol

Power supply corporations use the serial DNP 3.0 (Distributed Network Protocol) for the station and network control levels. SIPROTEC units function as DNP slaves, supplying their information to a master system or receiving information from it.

System solutions for protection and station control

Together with the SICAM power automation system, SIPROTEC 4 can be used with PROFIBUS DP. Over the low-cost electrical RS485 bus, or interference-free via the optical double ring, the units exchange information with the control system.

Units featuring IEC 60870-5-103 interfaces can be connected to SICAM in parallel via the RS485 bus or radially by fiber-optic link. Through this interface, the system is open for the connection of units of other manufacturers (see Fig. 5/68).

Because of the standardized interfaces, SIPROTEC units can also be integrated into systems of other manufacturers or in SIMATIC. Electrical RS485 or optical interfaces are available. The optimum physical data transfer medium can be chosen thanks to opto-electrical converters. Thus, the RS485 bus allows low-cost wiring in the cubicles and an interference-free optical connection to the master can be established.

For IEC 61850, an interoperable system solution is offered with SICAM PAS. Via the 100 Mbits/s Ethernet bus, the units are linked with PAS electrically or optically to the station PC. The interface is standardized, thus also enabling direct connection of units of other manufacturers to the Ethernet bus. With IEC 61850, however, the units can also be used in other manufacturers' systems (see Fig. 5/69).

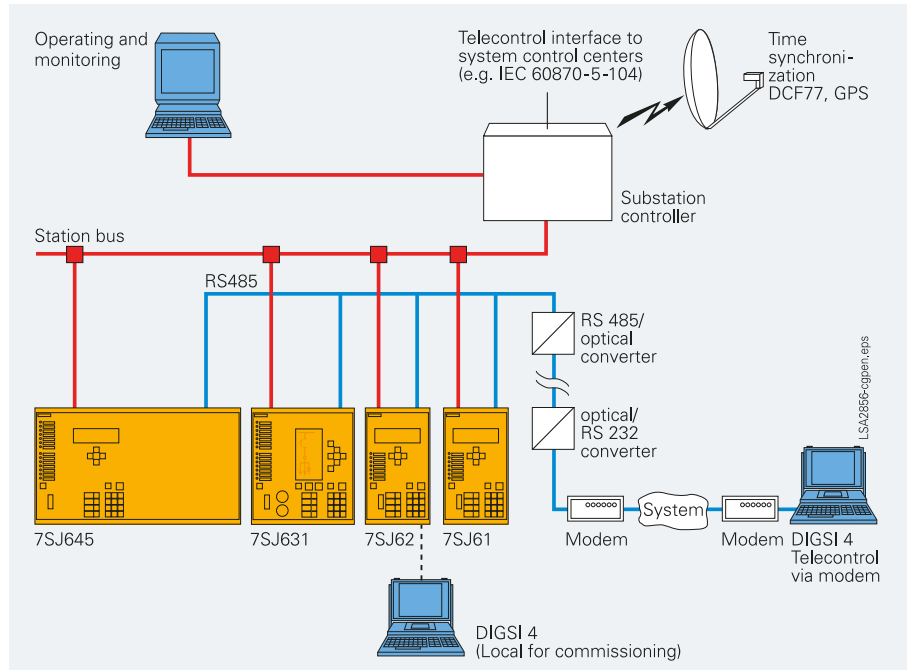


Fig. 5/70 System solution/communication

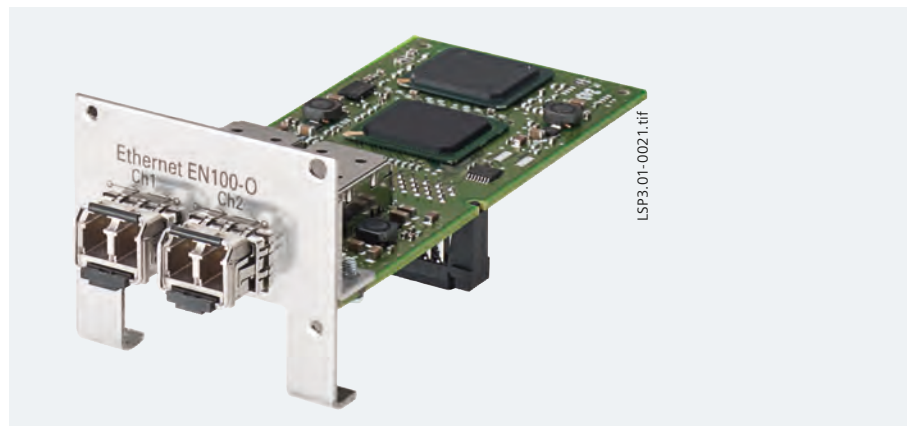


Fig. 5/71 Optical Ethernet communication module for IEC 61850 with integrated Ethernet-switch

Overcurrent Protection / 7SJ63

Typical connections

Typical connections

■ Connection of current and voltage transformers

Standard connection

For grounded networks, the ground current is obtained from the phase currents by the residual current circuit.

5

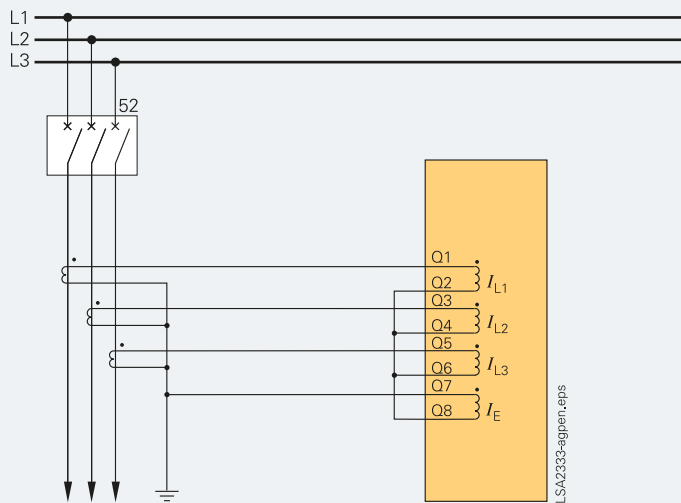


Fig. 5/72 Residual current circuit without directional element

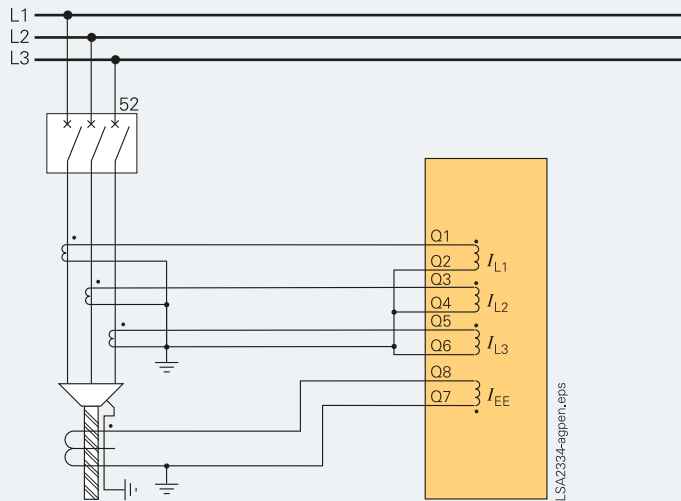


Fig. 5/73 Sensitive ground-current detection without directional element

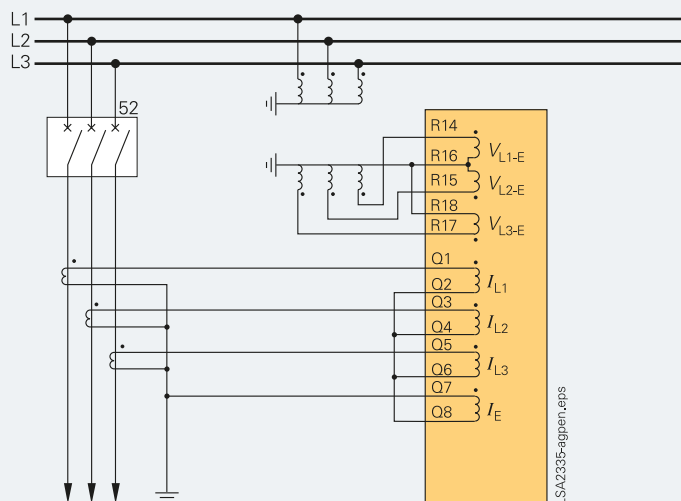


Fig. 5/74 Residual current circuit with directional element

Connection for compensated networks

The figure shows the connection of two phase-to-ground voltages and the V_E voltage of the open delta winding and a phase-balance neutral current transformer for the ground current. This connection maintains maximum precision for directional ground-fault detection and must be used in compensated networks. Figure 5/130 shows sensitive directional ground-fault detection.

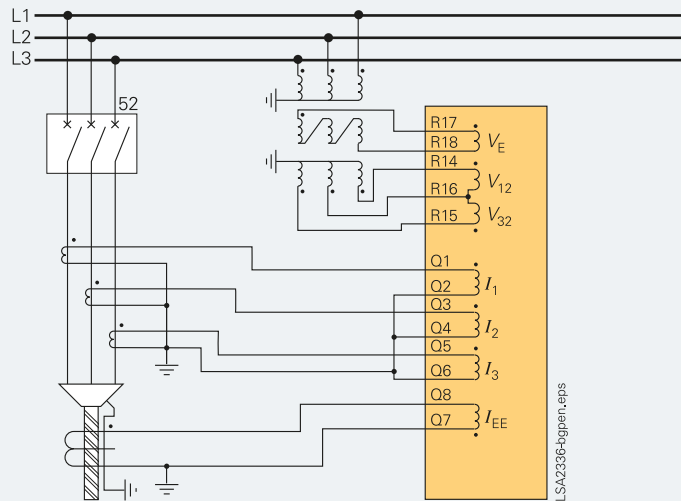


Fig. 5/75 Sensitive directional ground-fault detection with directional element for phases

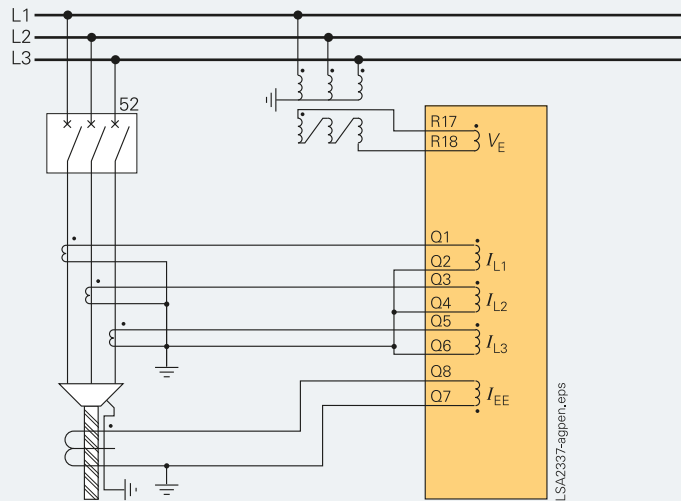


Fig. 5/76 Sensitive directional ground-fault detection

Connection for isolated-neutral or compensated networks only

If directional ground-fault protection is not used, the connection can be made with only two phase current transformers. Directional phase short-circuit protection can be achieved by using only two primary transformers.

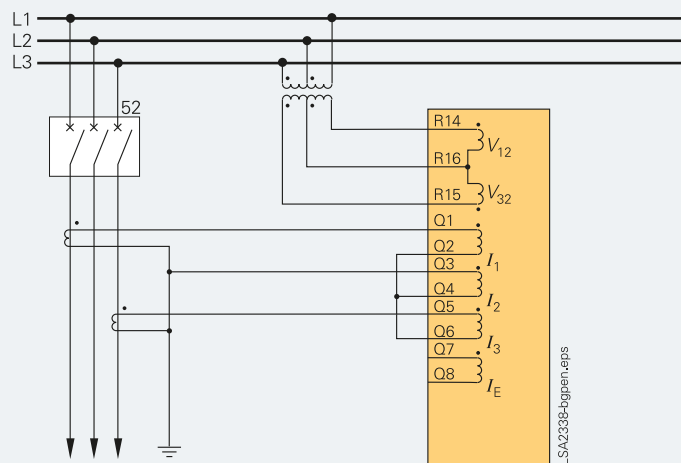


Fig. 5/77 Isolated-neutral or compensated networks

Overcurrent Protection / 7SJ63

Typical applications

5

Overview of connection types			
Type of network	Function	Current connection	Voltage connection
(Low-resistance) grounded network	Overcurrent protection phase/ground non-directional	Residual circuit, with 3 phase-current transformers required, phase-balance neutral current transformer possible	–
(Low-resistance) grounded networks	Sensitive ground-fault protection	Phase-balance neutral current transformers required	–
Isolated or compensated networks	Overcurrent protection phases non-directional	Residual circuit, with 3 or 2 phase current transformers possible	–
(Low-resistance) grounded networks	Overcurrent protection phases directional	Residual circuit, with 3 phase-current transformers possible	Phase-to-ground connection or phase-to-phase connection
Isolated or compensated networks	Overcurrent protection phases directional	Residual circuit, with 3 or 2 phase-current transformers possible	Phase-to-ground connection or phase-to-phase connection
(Low-resistance) grounded networks	Overcurrent protection ground directional	Residual circuit, with 3 phase-current transformers required, phase-balance neutral current transformers possible	Phase-to-ground connection required
Isolated networks	Sensitive ground-fault protection	Residual circuit, if ground current $> 0.05 I_N$ on secondary side, otherwise phase-balance neutral current transformers required	3 times phase-to-ground connection or phase-to-ground connection with open delta winding
Compensated networks	Sensitive ground-fault protection $\cos \varphi$ measurement	Phase-balance neutral current transformers required	Phase-to-ground connection with open delta winding required

Typical applications

■ Connection of circuit-breaker

Undervoltage releases

Undervoltage releases are used for automatic tripping of high-voltage motors.

Example:

DC supply voltage of control system fails and manual electric tripping is no longer possible.

Automatic tripping takes place when voltage across the coil drops below the trip limit. In Fig. 5/78, tripping occurs due to failure of DC supply voltage, by automatic opening of the live status contact upon failure of the protection unit or by short-circuiting the trip coil in event of a network fault

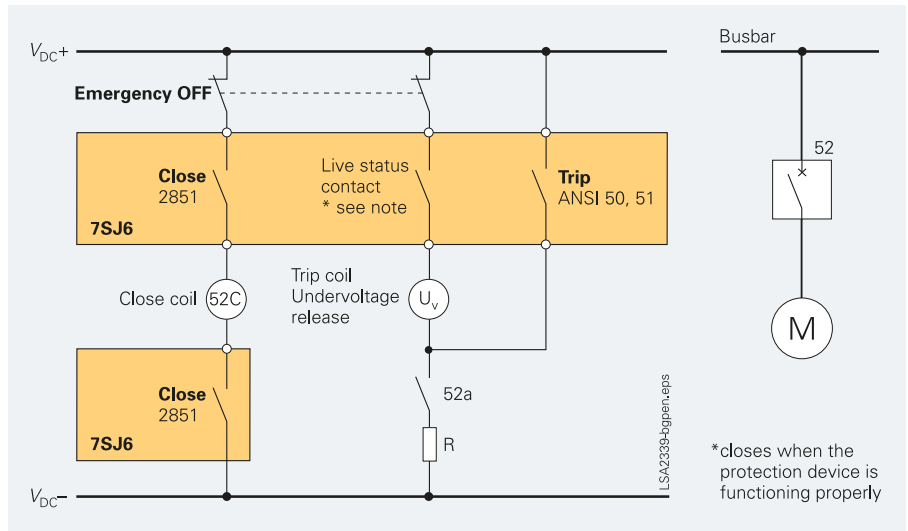


Fig. 5/78 Undervoltage release with make contact (50, 51)

In Fig. 5/79 tripping is by failure of auxiliary voltage and by interruption of tripping circuit in the event of network failure. Upon failure of the protection unit, the tripping circuit is also interrupted, since contact held by internal logic drops back into open position.

Trip circuit supervision (ANSI 74TC)

One or two binary inputs can be used for monitoring the circuit-breaker trip coil including its incoming cables. An alarm signal occurs whenever the circuit is interrupted.

Lockout (ANSI 86)

All binary outputs can be stored like LEDs and reset using the LED reset key. The lockout state is also stored in the event of supply voltage failure. Reclosure can only occur after the lockout state is reset.

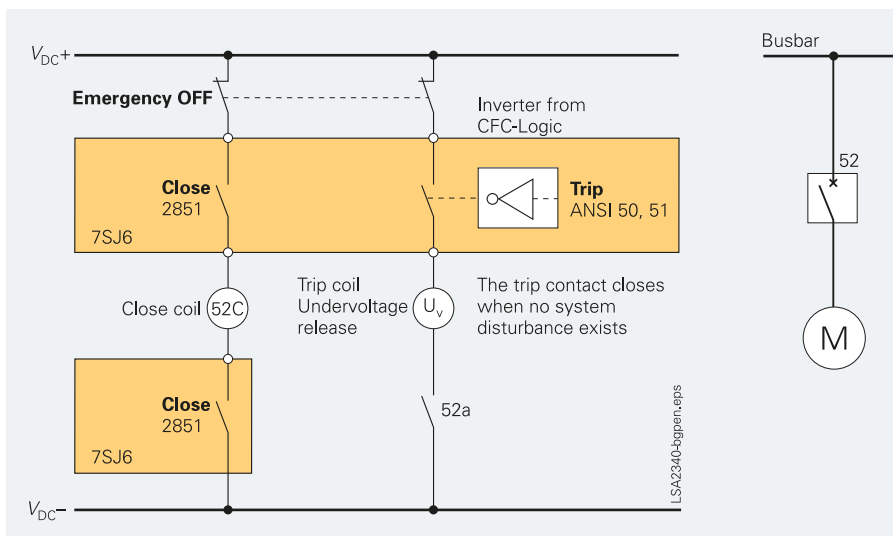


Fig. 5/79 Undervoltage release with locking contact (trip signal 50 is inverted)

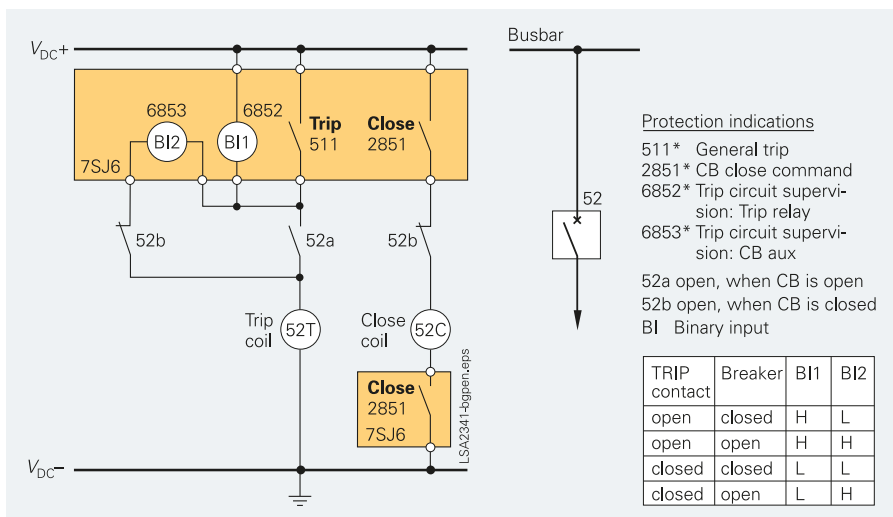


Fig. 5/80 Trip circuit supervision with 2 binary inputs

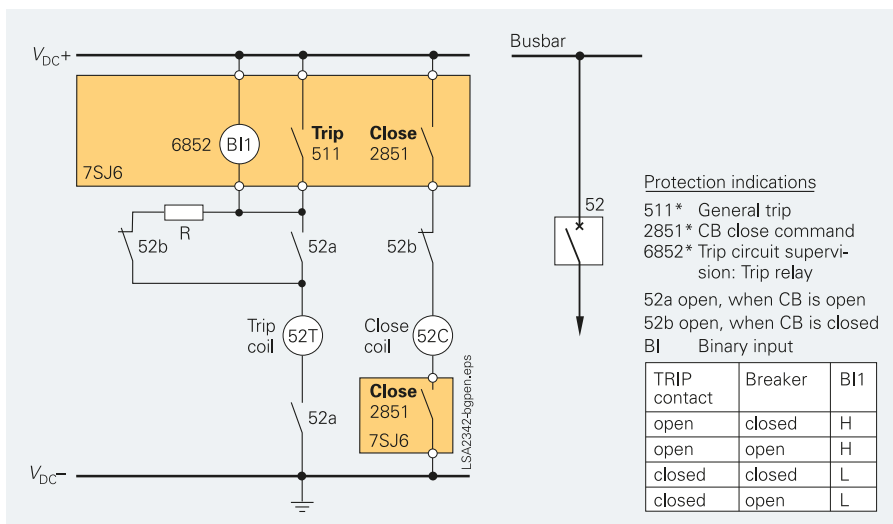


Fig. 5/81 Trip circuit supervision with 1 binary input

Overcurrent Protection / 7SJ63

Technical data

5

General unit data	
<i>Measuring circuits</i>	
System frequency	50 / 60 Hz (settable)
<i>Current transformer</i>	
Rated current I_{nom}	1 or 5 A (settable)
Option: sensitive ground-fault CT	$I_{EE} < 1.6$ A
Power consumption at $I_{nom} = 1$ A at $I_{nom} = 5$ A for sensitive ground-fault CT at 1 A	Approx. 0.05 VA per phase Approx. 0.3 VA per phase Approx. 0.05 VA
Overload capability Thermal (effective)	500 A for 1 s 150 A for 10 s 20 A continuous
Dynamic (impulse current)	$250 \times I_{nom}$ (half cycle)
Overload capability if equipped with sensitive ground-fault CT Thermal (effective)	300 A for 1 s 100 A for 10 s 15 A continuous
Dynamic (impulse current)	750 A (half cycle)
<i>Voltage transformer</i>	
Rated voltage V_{nom}	100 V to 225 V
Power consumption at $V_{nom} = 100$ V	< 0.3 VA per phase
Overload capability in voltage path (phase-neutral voltage) Thermal (effective)	230 V continuous
<i>Measuring transducer inputs</i>	
Type	7SJ633 7SJ636
Number	2 2
Input current	DC 0 – 20 mA
Input resistance	10 Ω
Power consumption	5.8 mW at 24 mA
<i>Auxiliary voltage (via integrated converter)</i>	
Rated auxiliary voltage V_{aux} DC	24/48 V 60/125 V 110/250 V
Permissible tolerance DC	19 – 58 V 48 – 150 V 88 – 300 V
Ripple voltage, peak-to-peak	≤ 12 % of rated auxiliary voltage
Power consumption	7SJ631 7SJ632 7SJ635 7SJ633 7SJ636
Quiescent Energized	Approx. 4 W 5.5 W 7 W Approx. 10 W 16 W 20 W
Backup time during loss/short-circuit of auxiliary direct voltage	≥ 50 ms at $V > DC 110$ V ≥ 20 ms at $V > DC 24$ V
Rated auxiliary voltage V_{aux} AC	115 V 230 V
Permissible tolerance AC	92 – 132 V 184 – 265 V
Power consumption	7SJ631 7SJ632 7SJ635 7SJ633 7SJ636
Quiescent Energized	Approx. 3 W 5 W 7 W Approx. 12 W 18 W 23 W
Backup time during loss/short-circuit of auxiliary alternating voltage	≥ 200 ms

Binary inputs/command inputs					
Type	7SJ631	7SJ632	7SJ633	7SJ635	7SJ636
Number (marshallable)	11	24	20	37	33
Voltage range	DC 24 – 250 V				
Pickup threshold modifiable by plug-in jumpers					
Pickup threshold DC	DC 19 V		DC 88 V		
For rated control voltage DC	24/48/60/110/ DC 125 V		DC 110/125/220/250 V		
Power consumption energized	0.9 mA (independent of operating voltage) for BI 1...6 / 8...19 / 25...36; 1.8 mA for BI 7 / 20...24 / 37				
Binary outputs/command outputs					
Type	7SJ631	7SJ632	7SJ633	7SJ635	7SJ636
Command/indication relay	8	11	11	14	14
Contacts per command/indication relay	1 NO / form A				
Live status contact	1 NO / NC (jumper) / form A / B				
Switching capacity					
Make	1000 W / VA				
Break	30 W / VA / 40 W resistive / 25 W at L/R ≤ 50 ms				
Switching voltage	$\leq DC 250$ V				
Permissible current	5 A continuous, 30 A for 0.5 s making current, 2000 switching cycles				
Power relay (for motor control)					
Type	7SJ631	7SJ632	7SJ633	7SJ635 7SJ636	
Number	0	2(4)	4 (8)		
Number of contacts/relay	2 NO / form A				
Switching capacity					
Make	1000 W / VA at 48 V ... 250 V / 500 W at 24 V				
Break	1000 W / VA at 48 V ... 250 V / 500 W at 24 V				
Switching voltage	$\leq DC 250$ V				
Permissible current	5 A continuous, 30 A for 0.5 s				

Electrical tests	
<i>Specification</i>	
Standards	IEC 60255 ANSI C37.90, C37.90.1, C37.90.2, UL508
<i>Insulation tests</i>	
Standards	IEC 60255-5; ANSI/IEEE C37.90.0
Voltage test (100 % test) all circuits except for auxiliary voltage and RS485/RS232 and time synchronization	2.5 kV (r.m.s. value), 50/60 Hz
Auxiliary voltage	DC 3.5 kV
Communication ports and time synchronization	AC 500 V
Impulse voltage test (type test) all circuits, except communication ports and time synchronization, class III	5 kV (peak value); 1.2/50 µs; 0.5 J 3 positive and 3 negative impulses at intervals of 5 s
<i>EMC tests for interference immunity; type tests</i>	
Standards	IEC 60255-6; IEC 60255-22 (product standard) EN 50082-2 (generic specification) DIN 57435 Part 303
High-frequency test IEC 60255-22-1, class III and VDE 0435 Part 303, class III	2.5 kV (peak value); 1 MHz; τ = 15 ms; 400 surges per s; test duration 2 s
Electrostatic discharge IEC 60255-22-2 class IV and EN 61000-4-2, class IV	8 kV contact discharge; 15 kV air gap discharge; both polarities; 150 pF; R _i = 330 Ω
Irradiation with radio-frequency field, non-modulated IEC 60255-22-3 (Report) class III	10 V/m; 27 to 500 MHz
Irradiation with radio-frequency field, amplitude-modulated IEC 61000-4-3; class III	10 V/m, 80 to 1000 MHz; AM 80 %; 1 kHz
Irradiation with radio-frequency field, pulse-modulated IEC 61000-4-3/ENV 50204; class III	10 V/m, 900 MHz; repetition rate 200 Hz, on duration 50 %
Fast transient interference/burst IEC 60255-22-4 and IEC 61000-4- 4, class IV	4 kV; 5/50 ns; 5 kHz; burst length = 15 ms; repetition rate 300 ms; both polarities; R _i = 50 Ω; test duration 1 min
High-energy surge voltages (Surge) IEC 61000-4-5; class III	
Auxiliary voltage	From circuit to circuit: 2 kV; 12 Ω; 9 µF across contacts: 1 kV; 2 Ω; 18 µF
Binary inputs/outputs	From circuit to circuit: 2 kV; 42 Ω; 0.5 µF across contacts: 1 kV; 42 Ω; 0.5 µF
Line-conducted HF, amplitude-modulated IEC 61000-4-6, class III	10 V; 150 kHz to 80 MHz; AM 80 %; 1 kHz
Power frequency magnetic field IEC 61000-4-8, class IV IEC 60255-6	30 A/m; 50 Hz, continuous 300 A/m; 50 Hz, 3 s 0.5 mT, 50 Hz
Oscillatory surge withstand capability ANSI/IEEE C37.90.1	2.5 to 3 kV (peak value), 1 to 1.5 MHz damped wave; 50 surges per s; duration 2 s, R _i = 150 to 200 Ω

Fast transient surge withstand capability ANSI/IEEE C37.90.1	4 to 5 kV; 10/150 ns; 50 surges per s both polarities; duration 2 s, R _i = 80 Ω
Radiated electromagnetic interference ANSI/IEEE C37.90.2	35 V/m; 25 to 1000 MHz; amplitude and pulse-modulated
Damped wave IEC 60694 / IEC 61000-4-12	2.5 kV (peak value, polarity alternating) 100 kHz, 1 MHz, 10 and 50 MHz, R _i = 200 Ω
<i>EMC tests for interference emission; type tests</i>	
Standard	EN 50081-* (generic specification)
Conducted interferences only auxiliary voltage IEC/CISPR 22	150 kHz to 30 MHz Limit class B
Radio interference field strength IEC/CISPR 11	30 to 1000 MHz Limit class B
Units with a detached operator panel must be installed in a metal cubicle to maintain limit class B	

Mechanical stress tests	
<i>Vibration, shock stress and seismic vibration</i>	
<u>During operation</u>	
Standards	IEC 60255-21 and IEC 60068-2
Vibration IEC 60255-21-1, class 2 IEC 60068-2-6	Sinusoidal 10 to 60 Hz; ± 0.075 mm amplitude; 60 to 150 Hz; 1 g acceleration frequency sweep 1 octave/min 20 cycles in 3 perpendicular axes
Shock IEC 60255-21-2, class 1 IEC 60068-2-27	Semi-sinusoidal Acceleration 5 g, duration 11 ms; 3 shocks in both directions of 3 axes
Seismic vibration IEC 60255-21-3, class 1 IEC 60068-3-3	Sinusoidal 1 to 8 Hz: ± 3.5 mm amplitude (horizontal axis) 1 to 8 Hz: ± 1.5 mm amplitude (vertical axis) 8 to 35 Hz: 1 g acceleration (horizontal axis) 8 to 35 Hz: 0.5 g acceleration (vertical axis) Frequency sweep 1 octave/min 1 cycle in 3 perpendicular axes
<u>During transportation</u>	
Standards	IEC 60255-21 and IEC 60068-2
Vibration IEC 60255-21-1, class 2 IEC 60068-2-6	Sinusoidal 5 to 8 Hz: ± 7.5 mm amplitude; 8 to 150 Hz; 2 g acceleration, frequency sweep 1 octave/min 20 cycles in 3 perpendicular axes
Shock IEC 60255-21-2, Class 1 IEC 60068-2-27	Semi-sinusoidal Acceleration 15 g, duration 11 ms 3 shocks in both directions of 3 axes
Continuous shock IEC 60255-21-2, class 1 IEC 60068-2-29	Semi-sinusoidal Acceleration 10 g, duration 16 ms 1000 shocks in both directions of 3 axes

Overcurrent Protection / 7SJ63

Technical data

Climatic stress tests

Temperatures

Type-tested acc. to IEC 60068-2-1 and -2, test Bd, for 16 h	-25 °C to +85 °C /-13 °F to +185 °F
Temporarily permissible operating temperature, tested for 96 h	-20 °C to +70 °C /-4 °F to +158 °F
Recommended permanent operating temperature acc. to IEC 60255-6 (Legibility of display may be impaired above +55 °C /+131 °F)	-5 °C to +55 °C /+25 °F to +131 °F
– Limiting temperature during permanent storage	-25 °C to +55 °C /-13 °F to +131 °F
– Limiting temperature during transport	-25 °C to +70 °C /-13 °F to +158 °F

Humidity

Permissible humidity It is recommended to arrange the units in such a way that they are not exposed to direct sunlight or pronounced temperature changes that could cause condensation.	Annual average 75 % relative humidity; on 56 days a year up to 95 % relative humidity; condensation not permissible!
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Unit design

Housing	7XP20	
Dimensions	See dimension drawings, part 14 of this catalog	
Weight in kg	Housing width 1/2	Housing width 1/1
Surface-mounting housing	7.5	15
Flush-mounting housing	6.5	13
Housing for detached operator panel	8.0	15
Detached operator panel	2.5	2.5
Degree of protection acc. to EN 60529	IP 51	
Surface-mounting housing	IP 51	
Flush-mounting housing	Front: IP 51, rear: IP 20;	
Operator safety	IP 2x with cover	

Further information can be found in the current manual at:
www.siemens.com/siprotec

Overcurrent Protection / 7SJ63

Selection and ordering data

5

Description			Order No.	Order code
7SJ63 multifunction protection relay			7SJ63 □ □ - □ □ □ □ □ □ - □ □ □ □	
Designation	ANSI No.	Description		
Basic version		Control		
	50/51	Overcurrent protection $I>$, $I>>$, I_p , reverse interlocking		
	50N/51N	Ground-fault protection $I_{E>}$, $I_{E>>}$, I_{EP}		
	50N/51N	Insensitive ground-fault protection via IEE function: $I_{EE>}$, $I_{EE>>}$, $I_{EEP}^{1)}$		
	49	Overload protection (with 2 time constants)		
	46	Phase balance current protection (negative-sequence protection)		
	37	Undercurrent monitoring		
	47	Phase sequence		
	59N/64	Displacement voltage		
	50BF	Breaker failure protection		
	74TC	Trip circuit supervision 4 setting groups, cold-load pickup Inrush blocking		
	86	Lockout		F A
■	V, f	27/59 Under-/overvoltage 810/U Under-/overfrequency		F E
■	IEF V, f	27/59 Under-/overvoltage 810/U Under-/overfrequency Intermittent ground fault		P E
■	Dir	67/67N Direction determination for overcurrent, phases and ground 47 Phase sequence		F C
■	Dir V, f	67/67N Direction determination for overcurrent, phases and ground 27/59 Under-/overvoltage 810/U Under-/overfrequency		F G
■	Dir IEF	67/67N Direction determination for overcurrent, phases and ground Intermittent ground fault		P C
Directional ground-fault detection	Dir	67/67N Direction determination for overcurrent, phases and ground 67Ns Directional sensitive ground-fault detection 87N High-impedance restricted ground fault		F D ²⁾
■	Dir IEF	67/67N Direction determination for overcurrent, phases and ground 67Ns Directional sensitive ground-fault detection 87N High-impedance restricted ground fault Intermittent ground fault		P D ²⁾
Directional ground-fault detection		67Ns Directional sensitive ground-fault detection 87N High-impedance restricted ground fault		F B ²⁾
■	Motor V, f	67Ns Directional sensitive ground-fault detection 87N High-impedance restricted ground fault detection 48/14 Starting time supervision, locked rotor		
■		66/86 Restart inhibit 27/59 Under-/overvoltage 810/U Under-/overfrequency		H F ²⁾

Continued on next page

- Basic version included
- V, f = Voltage, frequency protection
- Dir = Directional overcurrent protection
- IEF = Intermittent ground fault

- 1) Only with insensitive ground-current transformer when position 7 = 1, 5, 7.
- 2) For isolated / compensated networks only with sensitive ground-current transformer when position 7 = 2, 6.

Overcurrent Protection/7SJ63

Selection and ordering data

Description			Order No.	Order code
7SJ63 multifunction protection relay			7SJ63 □ □ - □ □ □ □ □ □ - □ □ □ □	
Designation	ANSI No.	Description		
Basic version		Control		
	50/51	Overcurrent protection $I>$, $I>>$, I_p , reverse interlocking		
	50N/51N	Ground-fault protection $I_{E>}$, $I_{E>>}$, I_{EP}		
	50N/51N	Ground-fault protection via insensitive IEE function: $I_{EE>}$, $I_{EE>>}$, $I_{EEP}^{1)}$		
	49	Overload protection (with 2 time constants)		
	46	Phase balance current protection (negative-sequence protection)		
	37	Undercurrent monitoring		
	47	Phase sequence		
	59N/64	Displacement voltage		
	50BF	Breaker failure protection		
	74TC	Trip circuit supervision 4 setting groups, cold-load pickup		
	86	Inrush blocking Lockout		
Directional Motor ground-fault Dir detection	V, f	67/67N Direction determination for overcurrent, phases and ground 67Ns Directional sensitive ground-fault detection 87N High-impedance restricted ground fault 48/14 Starting time supervision, locked rotor 66/86 Restart inhibit 27/59 Under-/overvoltage 81O/U Under-/overfrequency		H H ²⁾
Directional Motor IEF V, f ground-fault Dir detection	V, f	67/67N Direction determination for overcurrent, phases and ground 67Ns Directional sensitive ground-fault detection 87N High-impedance restricted ground fault Intermittent ground fault 48/14 Starting time supervision, locked rotor 66/86 Restart inhibit 27/59 Undervoltage/overvoltage 81O/U Underfrequency/overfrequency		R H ²⁾
■ Motor Dir	V, f	67/67N Direction determination for overcurrent, phases and ground 48/14 Starting time supervision, locked rotor 66/86 Restart inhibit 27/59 Under-/overvoltage 81O/U Under-/overfrequency		H G
■ Motor		48/14 Starting time supervision, locked rotor 66/86 Restart inhibit		H A
ARC, fault locator		Without 79 With auto-reclosure 21FL With fault locator 79, 21FL With auto-reclosure, with fault locator		0 1 2 3

■ Basic version included

V, f = Voltage, power, frequency protection

Dir = Directional overcurrent protection

IEF = Intermittent ground fault

1) Only with insensitive ground-current transformer when position 7 = 1, 5, 7.

2) For isolated / compensated networks only with sensitive ground-current transformer when position 7 = 2, 6.

Overcurrent Protection / 7SJ63

Selection and ordering data

Description	Order No.	Order code
7SJ63 multifunction protection relay	7SJ63 □ □ - □ □ □ □ - □ □ □ □ - □ □ □	
System interface (on rear of unit, Port B)		
No system interface	0	
IEC 60870-5-103 protocol, RS232	1	
IEC 60870-5-103 protocol, RS485	2	
IEC 60870-5-103 protocol, 820 nm fiber, ST connector	3	
PROFIBUS DP Slave, RS485	9	L O A
PROFIBUS DP Slave, 820 nm wavelength, double ring, ST connector ¹⁾	9	L O B
MODBUS, RS485	9	L O D
MODBUS, 820 nm wavelength, ST connector ²⁾	9	L O E
DNP 3.0, RS485	9	L O G
DNP 3.0, 820 nm wavelength, ST connector ²⁾	9	L O H
IEC 61850, 100 Mbit Ethernet, electrical, double, RJ45 connector (EN 100)	9	L O R
IEC 61850, 100 Mbit Ethernet, optical, double, LC connector (EN 100) ²⁾	9	L O S

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- 1) Not with position 9 = "B"; if 9 = "B", please order 7SJ6 unit with RS485 port and separate fiber-optic converters.
 For single ring, please order converter 6GK1502-3AB10, not available with position 9 = "B".
 For double ring, please order converter 6GK1502-4AB10, not available with position 9 = "B".
 The converter requires a AC 24 V power supply (e.g. power supply 7XV5810-0BA00).
- 2) Not available with position 9 = "B".

Sample order

Position	Order No. + Order code
	7SJ632 5 - 5 E C 9 1 - 3 F C 1 + L O G
6 I/O's: 24 BI/11 BO, 1 live status contact	2
7 Current transformer: 5 A	5
8 Power supply: DC 110 to 250 V, AC 115 V to AC 230 V	5
9 Unit version: Flush-mounting housing, screw-type terminals	E
10 Region: US, English language (US); 60 Hz, ANSI	C
11 Communication: System interface: DNP 3.0, RS485	9
12 Communication: DIGSI 4, electric RS232	1
13 Measuring/fault recording: Extended measuring and fault records	3
14/15 Protection function package: Basic version plus directional TOC	F C
16 With auto-reclosure	1



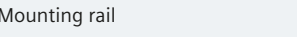
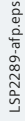




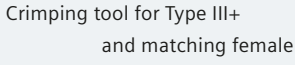
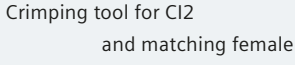

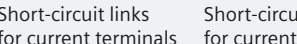
Overcurrent Protection/7SJ63

Selection and ordering data

Accessories	Description	Order No.
	Temperature monitoring box AC/DC 24 to 60 V AC/DC 90 to 240 V	7XV5662-2AD10 7XV5662-5AD10
	Varistor/VoltageArrester Voltage arrester for high-impedance REF protection 125 Vrms; 600 A; 1S/S 256 240 Vrms; 600 A; 1S/S 1088	C53207-A401-D76-1 C53207-A401-D77-1
	Connecting cable Cable between PC/notebook (9-pin con.) and protection unit (9-pin connector) (contained in DIGSI 4, but can be ordered additionally) Cable between temperature monitoring box and SIPROTEC 4 unit - length 5 m / 16.4 ft - length 25 m / 82 ft - length 50 m / 164 ft	7XV5100-4 7XV5103-7AA05 7XV5103-7AA25 7XV5103-7AA50
	Manual for 7SJ63 English/German	C53000-G1140-C147-x ¹⁾
	1) x = please inquire for latest edition (exact Order No.).	

Overcurrent Protection / 7SJ63

Selection and ordering data

Accessories	Description	Order No.	Size of package	Supplier	
   Mounting rail	Terminal safety cover				
	Voltage/current terminal 18-pole/12-pole	C73334-A1-C31-1	1	Siemens	
  2-pin connector	Voltage/current terminal 12-pole/8-pole	C73334-A1-C32-1	1	Siemens	
	Connector 2-pin	C73334-A1-C35-1	1	Siemens	
	Connector 3-pin	C73334-A1-C36-1	1	Siemens	
	 3-pin connector	Crimp connector CI2 0.5 to 1 mm ²	0-827039-1	4000 taped on reel	1))
 Short-circuit links for current terminals	Crimp connector CI2 0.5 to 1 mm ²	0-827396-1	1	1)	
	 Short-circuit links for current terminals	Crimp connector: Type III+ 0.75 to 1.5 mm ²	0-163084-2	1	1)
		Crimp connector: Type III+ 0.75 to 1.5 mm ²	0-163083-7	4000 taped on reel	1)
	 Crimping tool for Type III+ and matching female	Crimping tool for CI2	0-539635-1	1	1)
		Crimping tool for CI2 and matching female	0-539668-2	1	1)
	 Crimping tool for CI2 and matching female	Short-circuit links for current terminals	0-734372-1	1	1)
Short-circuit links for other terminals		1-734387-1	1	1)	
 Short-circuit links for current terminals	Short-circuit links for current terminals	C73334-A1-C33-1	1	Siemens	
	Short-circuit links for other terminals	C73334-A1-C34-1	1	Siemens	
 Mounting rail for 19" rack	Mounting rail for 19" rack	C73165-A63-D200-1	1	Siemens	

1) Your local Siemens representative can inform you on local suppliers.

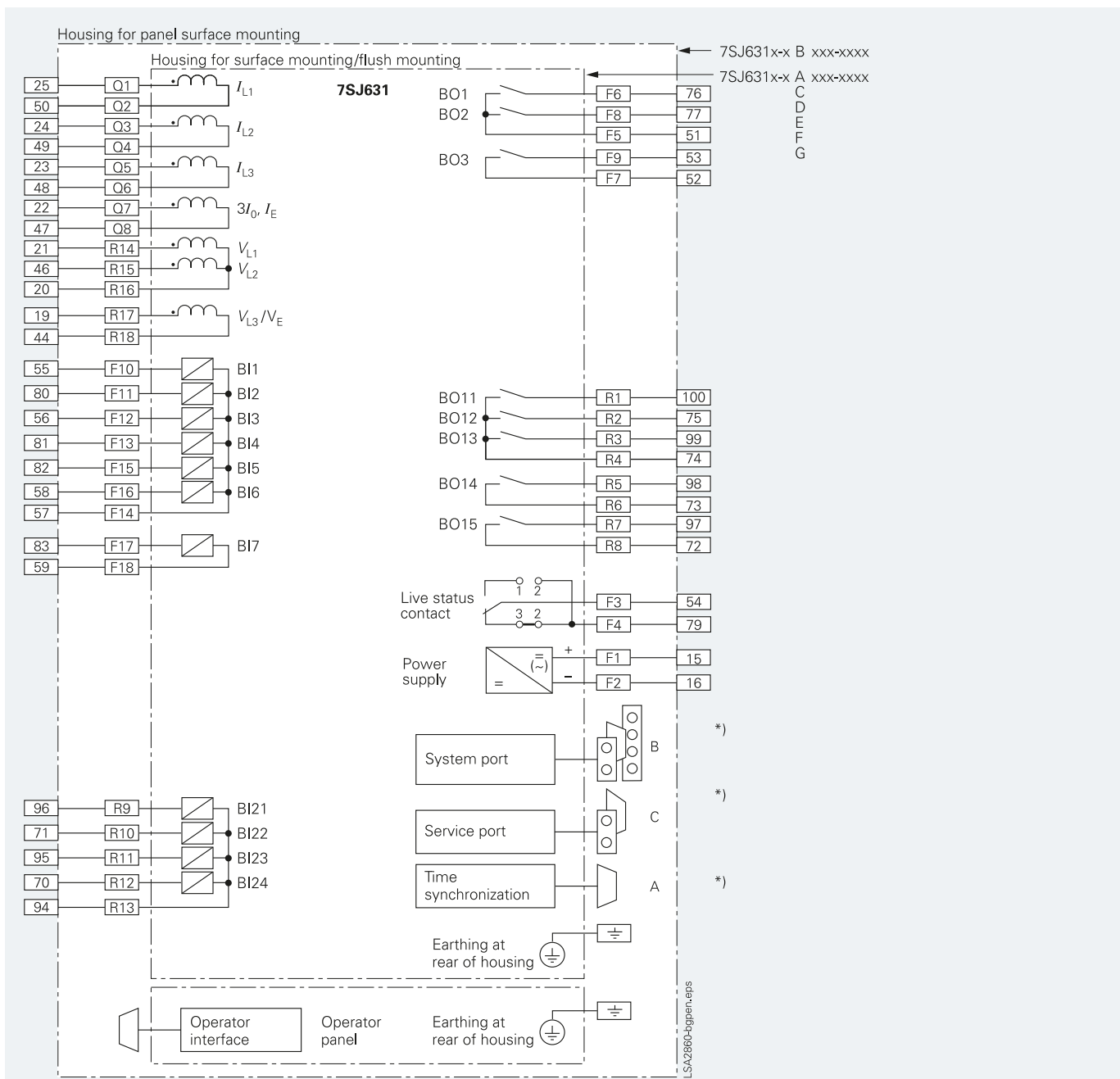
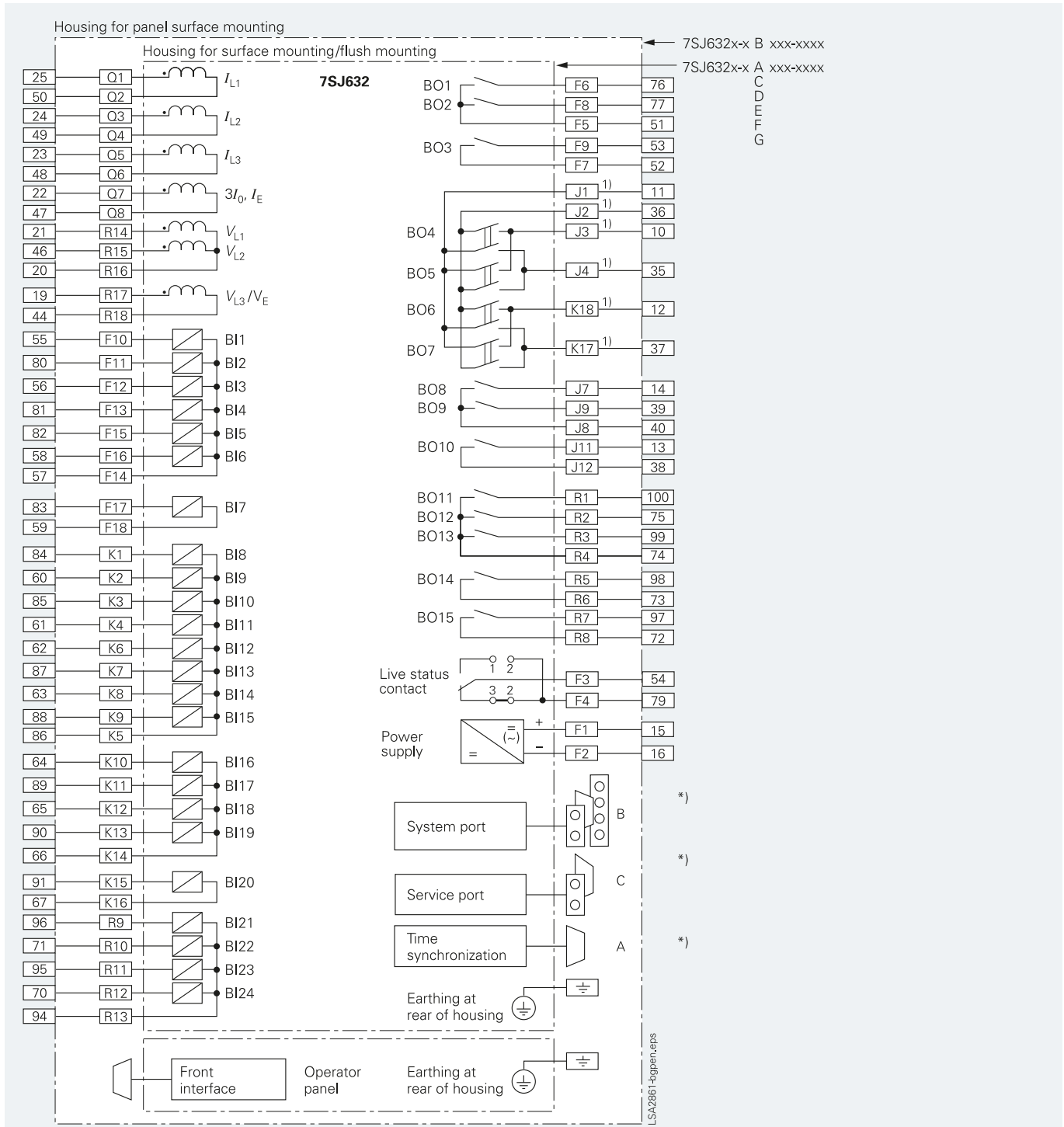


Fig. 5/82 7SJ631 connection diagram

Overcurrent Protection / 7SJ63

Connection diagram

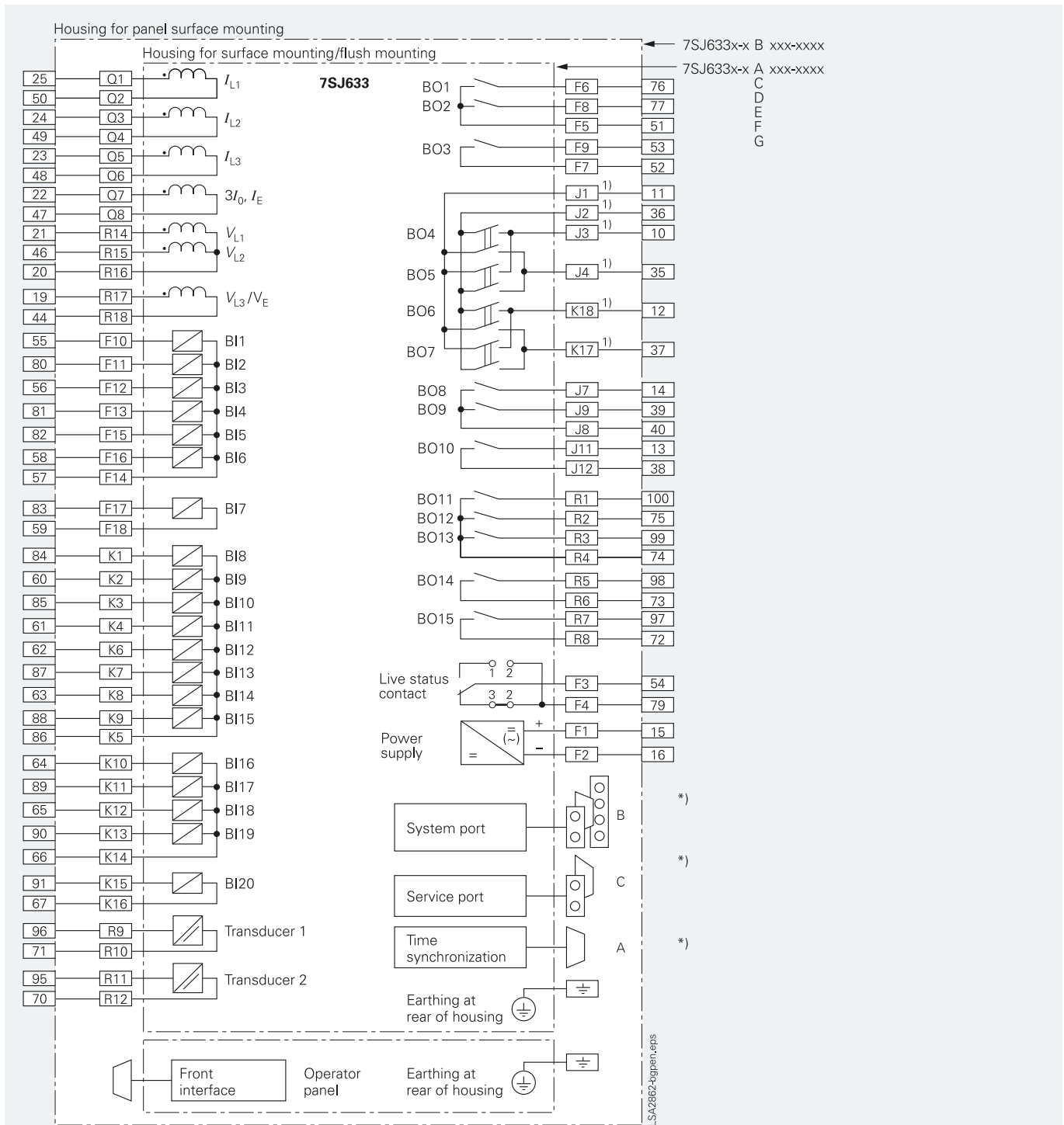
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*) For pinout of communication ports see part 14 of this catalog.
For the allocation of the terminals of the panel surface-mounting version refer to the manual (<http://www.siemens.com/siprotec>).

1) Power relays are intended to directly control motorized switches. The power relays are interlocked so only one relay of each pair can close at a time, in order to avoid shorting out the power supply. The power relay pairs are BO4/BO5, BO6/BO7. If used for protection purposes only one binary output of a pair can be used.

Fig. 5/83 7SJ632 connection diagram



*) For pinout of communication ports see part 14 of this catalog.
 For the allocation of the terminals of the panel surface-mounting version refer to the manual (<http://www.siemens.com/siprotec>).

1) Power relays are intended to directly control motorized switches. The power relays are interlocked so only one relay of each pair can close at a time, in order to avoid shorting out the power supply. The power relay pairs are BO4/BO5, BO6/BO7. If used for protection purposes only one binary output of a pair can be used.

Fig. 5/84 7SJ633 connection diagram

Overcurrent Protection / 7SJ63

Connection diagram

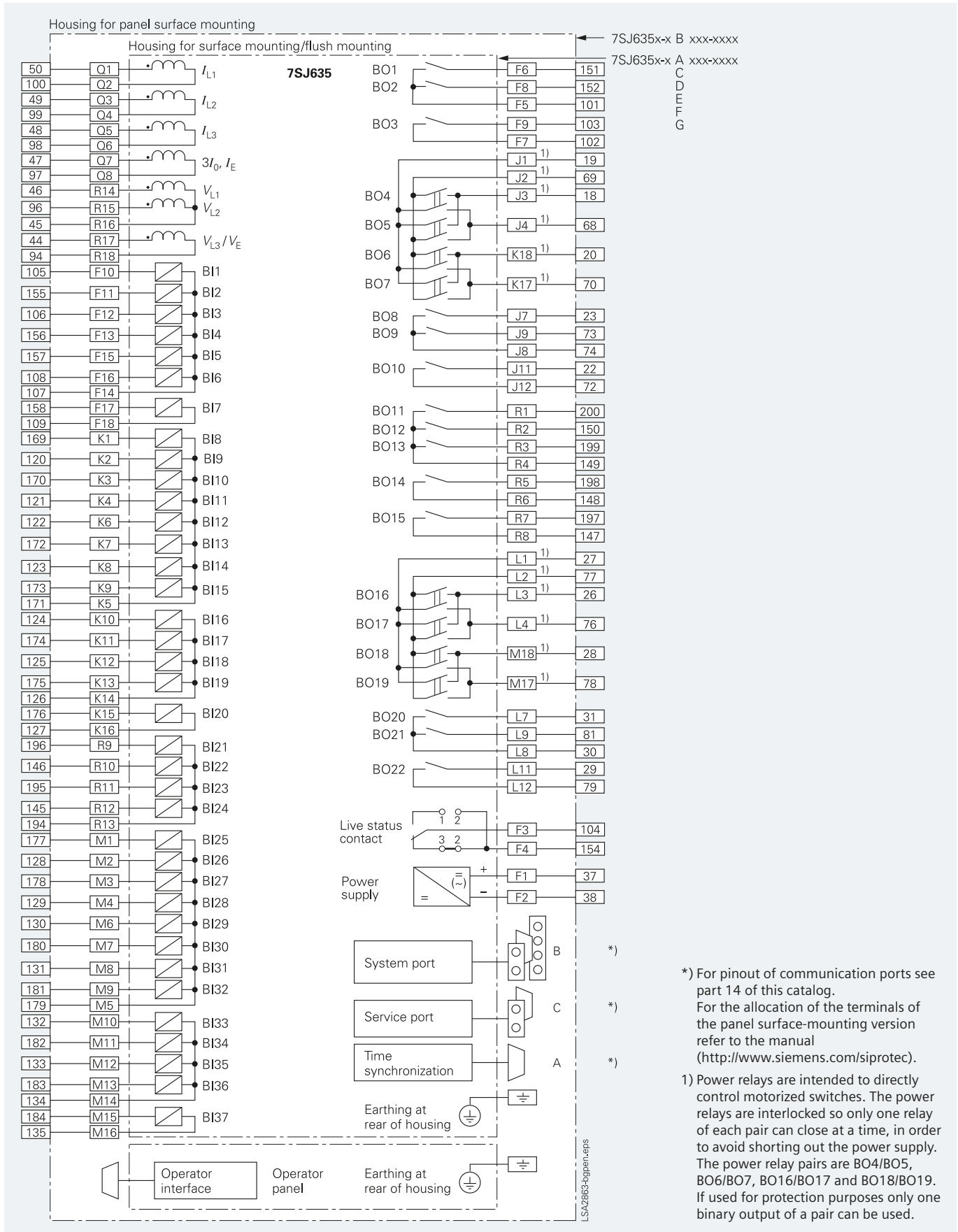


Fig. 5/85 7SJ635 connection diagram

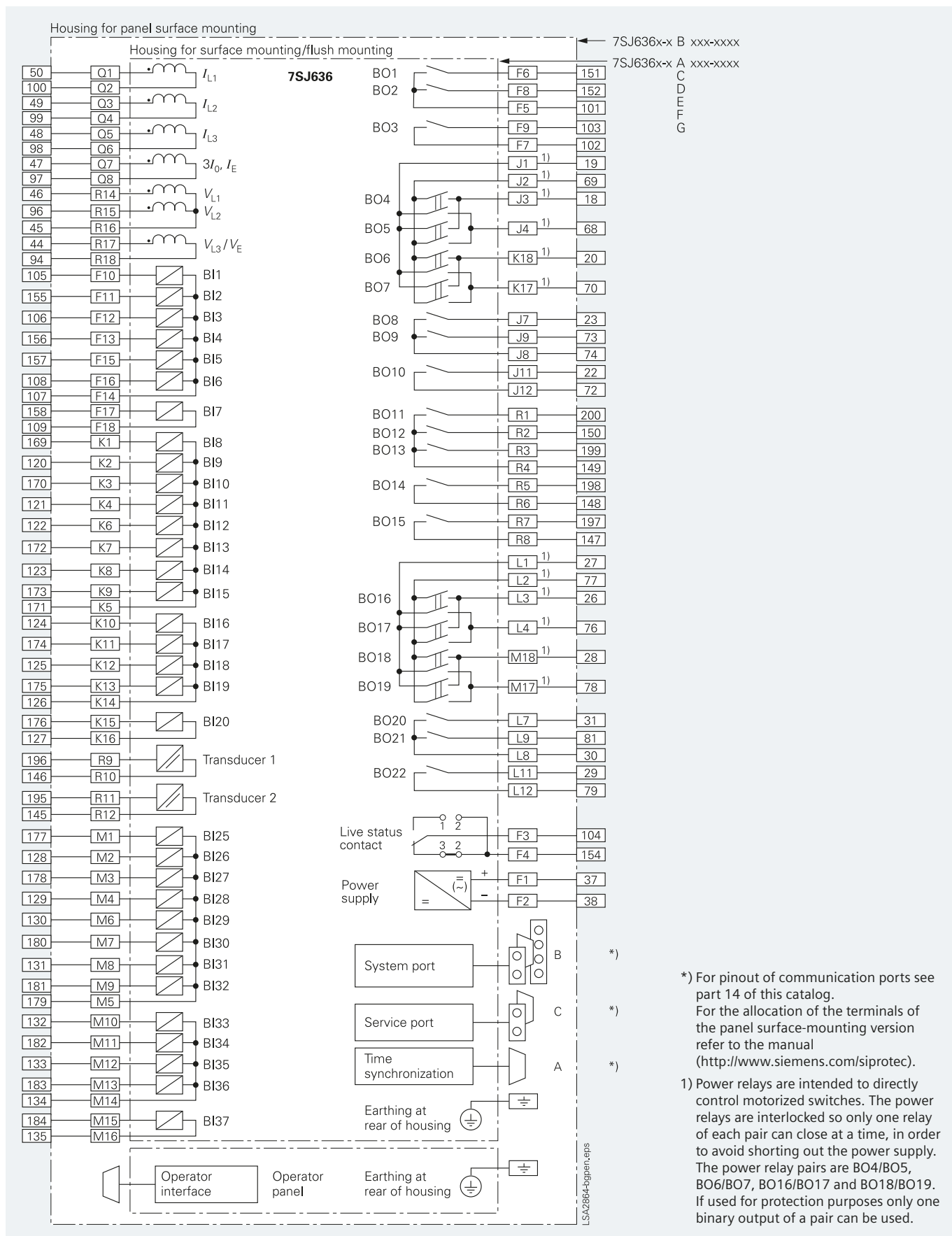


Fig. 5/86 7SJ636 connection diagram