



Fig. 5/20 Multifunction protection relay with text (left) and graphic display

### Protection functions (continued)

- Inrush restraint
- Motor protection
- Overload protection
- Temperature monitoring
- Under-/overvoltage protection
- Under-/overfrequency protection
- Rate-of-frequency-change protection
- Power protection (e.g. reverse, factor)
- Undervoltage controlled reactive power protection
- Breaker failure protection
- Negative-sequence protection
- Phase-sequence monitoring
- Synchro-check
- Fault locator
- Lockout
- Auto-reclosure

### Description

The SIPROTEC 7SJ62 relays can be used for line protection of high and medium voltage networks with earthed (grounded), low-resistance grounded, isolated or compensated neutral point. With regard to motor protection, the SIPROTEC 7SJ62 is suitable for asynchronous machines of all sizes. The relay performs all functions of backup protection supplementary to transformer differential protection.

7SJ62 is featuring the "flexible protection functions". Up to 20 protection functions can be added according to individual requirements. Thus, for example, a rate-of-frequency-change protection or reverse power protection can be implemented.

The relay provides control of the circuit-breaker, further switching devices and automation functions. The integrated programmable logic (CFC) allows the user to implement their own functions, e. g. for the automation of switchgear (interlocking). The user is also allowed to generate user-defined messages.

The flexible communication interfaces are open for modern communication architectures with control systems.

### Function overview

#### Protection functions

- Overcurrent protection
- Directional overcurrent protection
- Sensitive directional ground-fault detection
- Displacement voltage
- Intermittent ground-fault protection
- Directional intermittent ground fault protection
- High-impedance restricted ground fault

#### Control functions/programmable logic

- Commands f. ctrl of CB and of isolators
- Position of switching elements is shown on the graphic display
- Control via keyboard, binary inputs, DIGSI 4 or SCADA system
- User-defined logic with CFC (e.g. interlocking)

#### Monitoring functions

- Operational measured values  $V, I, f$
- Energy metering values  $W_p, W_q$
- Circuit-breaker wear monitoring
- Slave pointer
- Trip circuit supervision
- Fuse failure monitor
- 8 oscillographic fault records
- Motor statistics

#### Communication interfaces

- System interface
  - IEC 60870-5-103 / IEC 61850
  - PROFIBUS DP
  - DNP 3/DNP3 TCP/MODBUS RTU
  - PROFINET
- Service interface for DIGSI 4 (modem)
- Front interface for DIGSI 4
- Time synchronization via IRIG B/DCF77

#### Hardware

- 4 current transformers
- 3/4 voltage transformers
- 8/11 binary inputs
- 8/6 output relays

# Overcurrent Protection / 7SJ62

## Application

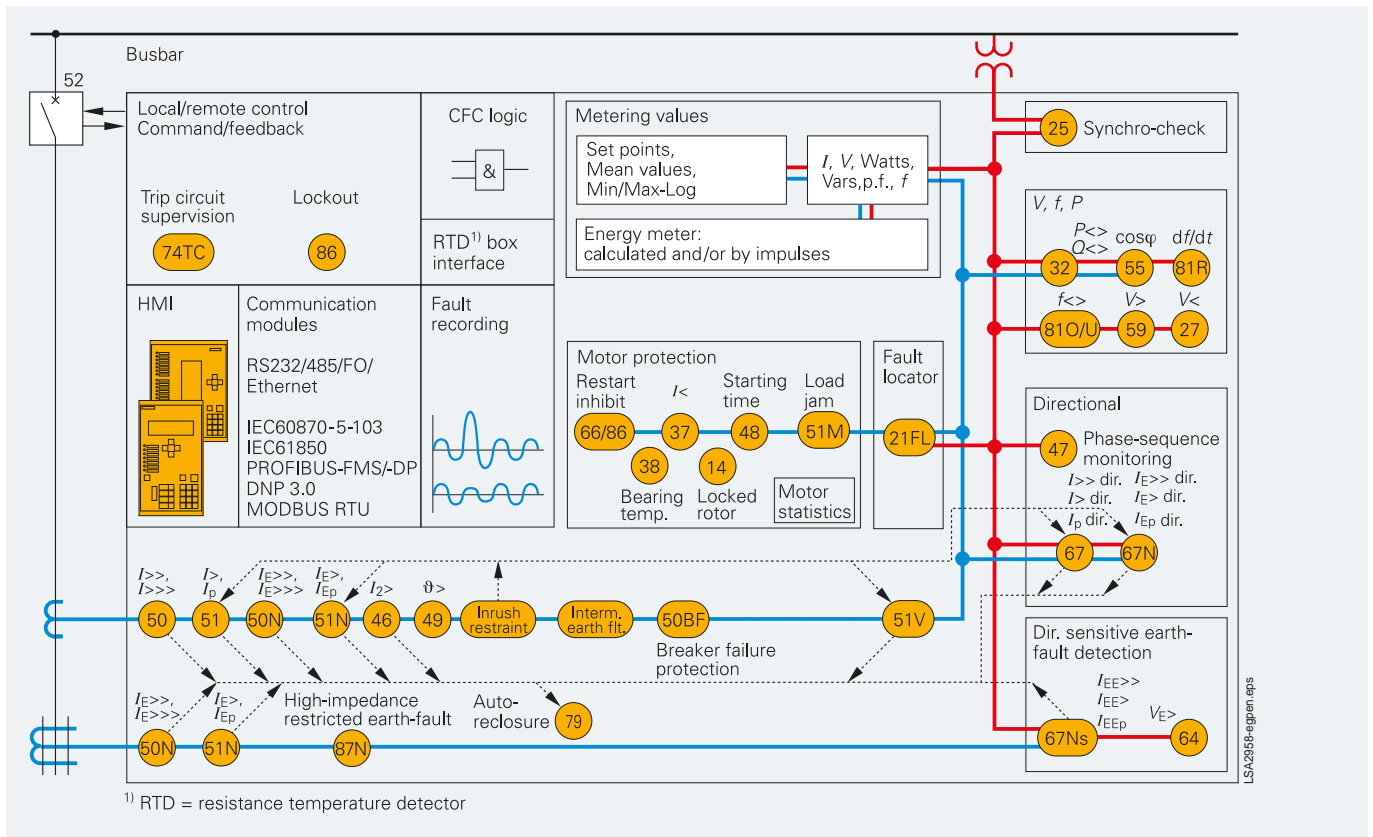


Fig. 5/21 Function diagram

### Application

The SIPROTEC 7SJ62 unit is a numerical protection relay that also performs control and monitoring functions and therefore supports the user in cost-effective power system management, and ensures reliable supply of electric power to the customers. Local operation has been designed according to ergonomic criteria. A large, easy-to-read display was a major design aim.

### Control

The integrated control function permits control of disconnect devices, grounding switches or circuit-breakers via the integrated operator panel, binary inputs, DIGSI 4 or the control and protection system (e.g. SICAM). The present status (or position) of the primary equipment can be displayed, in case of devices with graphic display. A full range of command processing functions is provided.

### Programmable logic

The integrated logic characteristics (CFC) allow the user to implement their own functions for automation of switchgear (interlocking) or a substation via a graphic user interface. The user can also generate user-defined messages.

### Line protection

The 7SJ62 units can be used for line protection of high and medium-voltage networks with earthed (grounded), low-resistance grounded, isolated or compensated neutral point.

### Synchro-check

In order to connect two components of a power system, the relay provides a synchro-check function which verifies that switching ON does not endanger the stability of the power system.

### Motor protection

When protecting motors, the 7SJ62 relay is suitable for asynchronous machines of all sizes.

### Transformer protection

The relay performs all functions of backup protection supplementary to transformer differential protection. The inrush suppression effectively prevents tripping by inrush currents. The high-impedance restricted ground-fault protection detects short-circuits and insulation faults on the transformer.

### Backup protection

The 7SJ62 can be used universally for backup protection.

### Flexible protection functions

By configuring a connection between a standard protection logic and any measured or derived quantity, the functional scope of the relays can be easily expanded by up to 20 protection stages or protection functions.

### Metering values

Extensive measured values, limit values and metered values permit improved system management.

ANSI	IEC	Protection functions
50, 50N	$I>, I>>, I>>>, I_E>, I_E>>, I_E>>>$	Definite-time overcurrent protection (phase/neutral)
50, 51V, 51N	$I_p, I_{Ep}$	Inverse overcurrent protection (phase/neutral), phase function with voltage-dependent option
67, 67N	$I_{dir}>, I_{dir}>>, I_{p\ dir}$ $I_{Edir}>, I_{Edir}>>, I_{Ep\ dir}$	Directional overcurrent protection (definite/inverse, phase/neutral), Directional comparison protection
67Ns/50Ns	$I_{EE}>, I_{EE}>>, I_{EEp}$	Directional / non-directional sensitive ground-fault detection
–		Cold load pick-up (dynamic setting change)
59N/64	$V_E, V_{0>}$	Displacement voltage, zero-sequence voltage
–	$I_{IE}>$	Intermittent ground fault
67Ns	$I_{IE\ dir}>$	Directional intermittent ground fault protection
87N		High-impedance restricted ground-fault protection
50BF		Breaker failure protection
79		Auto-reclosure
25		Synchro-check
46	$I_2>$	Phase-balance current protection (negative-sequence protection)
47	$V_2>, \text{phase-sequence}$	Unbalance-voltage protection and/or phase-sequence monitoring
49	$\vartheta>$	Thermal overload protection
48		Starting time supervision
51M		Load jam protection
14		Locked rotor protection
66/86		Restart inhibit
37	$I<$	Undercurrent monitoring
38		Temperature monitoring via external device (RTD-box), e.g. bearing temperature monitoring
27, 59	$V<, V>$	Undervoltage / overvoltage protection
59R	$dV/dt$	Rate-of-voltage-change protection
32	$P<>, Q<>$	Reverse-power, forward-power protection
27/Q	$Q>/V<$	Undervoltage-controlled reactive power protection
55	$\cos \varphi$	Power factor protection
81O/U	$f>, f<$	Overfrequency / underfrequency protection
81R	$df/dt$	Rate-of-frequency-change protection
21FL		Fault locator

# Overcurrent Protection / 7SJ62

## Construction, protection functions



Fig. 5/22 Rear view with screw-type terminals, 1/3-rack size

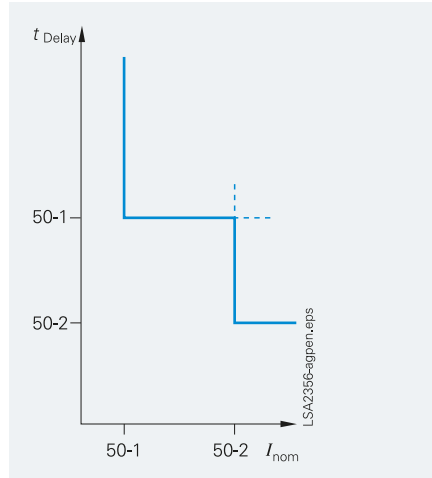


Fig. 5/23 Definite-time overcurrent protection

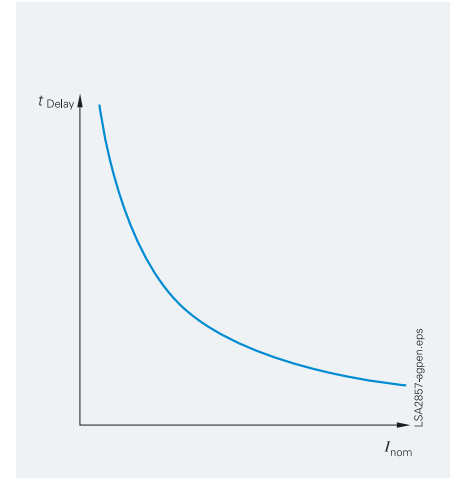


Fig. 5/24 Inverse-time overcurrent protection

5

### Construction

#### Connection techniques and housing with many advantages

1/3-rack size (text display variants) and 1/2-rack size (graphic display variants) are the available housing widths of the 7SJ62 relays, referred to a 19" module frame system. This means that previous models can always be replaced. The height is a uniform 244 mm for flush-mounting housings and 266 mm for surface-mounting housing. All cables can be connected with or without ring lugs.

In the case of surface mounting on a panel, the connection terminals are located above and below in the form of screw-type terminals. The communication interfaces are located in a sloped case at the top and bottom of the housing.

### Protection functions

#### Overcurrent protection (ANSI 50, 50N, 51, 51V, 51N)

This function is based on the phase-selective measurement of the three phase currents and the ground current (four transformers). Three definite-time overcurrent protection elements (DMT) exist both for the phases and for the ground. The current threshold and the delay time can be set within a wide range. In addition, inverse-time overcurrent protection characteristics (IDMTL) can be activated.

The inverse-time function provides – as an option – voltage-restraint or voltage-controlled operating modes.

### Available inverse-time characteristics

Characteristics acc. to	ANSI/IEEE	IEC 60255-3
Inverse	•	•
Short inverse	•	
Long inverse	•	•
Moderately inverse	•	
Very inverse	•	•
Extremely inverse	•	•

### Reset characteristics

For easier time coordination with electromechanical relays, reset characteristics according to ANSI C37.112 and IEC 60255-3 / BS 142 standards are applied.

When using the reset characteristic (disk emulation), a reset process is initiated after the fault current has disappeared. This reset process corresponds to the reverse movement of the Ferraris disk of an electromechanical relay (thus: disk emulation).

### User-definable characteristics

Instead of the predefined time characteristics according to ANSI, tripping characteristics can be defined by the user for phase and ground units separately. Up to 20 current/time value pairs may be programmed. They are set as pairs of numbers or graphically in DIGSI 4.

### Inrush restraint

The relay features second harmonic restraint. If the second harmonic is detected during transformer energization, pickup of non-directional and directional normal elements are blocked.

### Cold load pickup/dynamic setting change

For directional and non-directional overcurrent protection functions the initiation thresholds and tripping times can be switched via binary inputs or by time control.

### Directional overcurrent protection (ANSI 67, 67N)

Directional phase and ground protection are separate functions. They operate in parallel to the non-directional overcurrent elements. Their pickup values and delay times can be set separately. Definite-time and inverse-time characteristics are offered. The tripping characteristic can be rotated about  $\pm 180$  degrees.

By means of voltage memory, directionality can be determined reliably even for close-in (local) faults. If the switching device closes onto a fault and the voltage is too low to determine direction, directionality (directional decision) is made with voltage from the voltage memory. If no voltage exists in the memory, tripping occurs according to the coordination schedule.

For ground protection, users can choose whether the direction is to be determined via zero-sequence system or negative-sequence system quantities (selectable). Using negative-sequence variables can be advantageous in cases where the zero voltage tends to be very low due to unfavorable zero-sequence impedances.

### Directional comparison protection (cross-coupling)

It is used for selective protection of sections fed from two sources with instantaneous tripping, i.e. without the disadvantage of time coordination. The directional comparison protection is suitable if the distances between the protection stations are not significant and pilot wires are available for signal transmission. In addition to the directional comparison protection, the directional coordinated overcurrent protection is used for complete selective backup protection. If operated in a closed-circuit connection, an interruption of the transmission line is detected.

### (Sensitive) directional ground-fault detection (ANSI 64, 67Ns, 67N)

For isolated-neutral and compensated networks, the direction of power flow in the zero sequence is calculated from the zero-sequence current  $I_0$  and zero-sequence voltage  $V_0$ .

For networks with an isolated neutral, the reactive current component is evaluated; for compensated networks, the active current component or residual resistive current is evaluated. For special network conditions, e.g. high-resistance grounded networks with ohmic-capacitive ground-fault current or low-resistance grounded networks with ohmic-inductive current, the tripping characteristics can be rotated approximately  $\pm 45$  degrees.

Two modes of ground-fault direction detection can be implemented: tripping or "signalling only mode".

It has the following functions:

- TRIP via the displacement voltage  $V_E$ .
- Two instantaneous elements or one instantaneous plus one user-defined characteristic.
- Each element can be set in forward, reverse, or non-directional.
- The function can also be operated in the insensitive mode as an additional short-circuit protection.

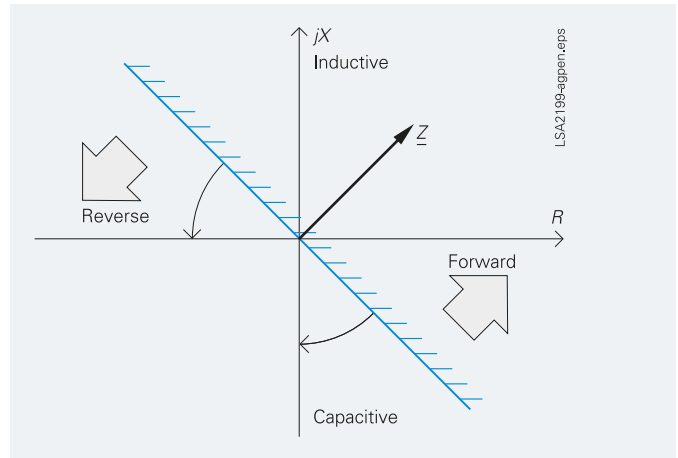


Fig. 5/25 Directional characteristic of the directional overcurrent protection

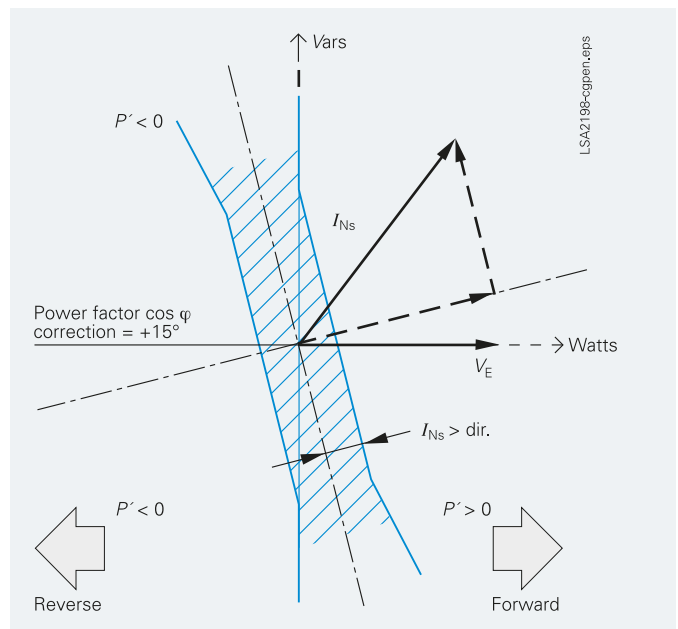


Fig. 5/26 Directional determination using cosine measurements for compensated networks

### (Sensitive) ground-fault detection (ANSI 50Ns, 51Ns / 50N, 51N)

For high-resistance grounded networks, a sensitive input transformer is connected to a phase-balance neutral current transformer (also called core-balance CT).

The function can also be operated in the insensitive mode as an additional short-circuit protection.

# Overcurrent Protection / 7SJ62

## Protection functions

### Intermittent ground-fault protection

Intermittent (re-striking) faults occur due to insulation weaknesses in cables or as a result of water penetrating cable joints. Such faults either simply cease at some stage or develop into lasting short-circuits. During intermittent activity, however, star-point resistors in networks that are impedance-grounded may undergo thermal overloading. The normal ground-fault protection cannot reliably detect and interrupt the current pulses, some of which can be very brief.

The selectivity required with intermittent ground faults is achieved by summing the duration of the individual pulses and by triggering when a (settable) summed time is reached. The response threshold  $I_{IE}$  evaluates the r.m.s. value, referred to one systems period.

### Directional intermittent ground fault protection (ANSI 67Ns)

The directional intermittent ground fault protection has to detect intermittent ground faults in resonant grounded cable systems selectively. Intermittent ground faults in resonant grounded cable systems are usually characterized by the following properties:

- A very short high-current ground current pulse (up to several hundred amperes) with a duration of under 1 ms
- They are self-extinguishing and re-ignite within one halfperiod up to several periods, depending on the power system conditions and the fault characteristic.
- Over longer periods (many seconds to minutes), they can develop into static faults.

Such intermittent ground faults are frequently caused by weak insulation, e.g. due to decreased water resistance of old cables. Ground fault functions based on fundamental component measured values are primarily designed to detect static ground faults and do not always behave correctly in case of intermittent ground faults. The function described here evaluates specifically the ground current pulses and puts them into relation with the zero-sequence voltage to determine the direction.

### Phase-balance current protection (ANSI 46) (Negative-sequence protection)

In line protection, the two-element phase-balance current/negative-sequence protection permits detection on the high side of high-resistance phase-to-phase faults and phase-to-ground faults that are on the low side of a transformer (e.g. with the switch group Dy 5). This provides backup protection for high-resistance faults beyond the transformer.

### Breaker failure protection (ANSI 50BF)

If a faulted portion of the electrical circuit is not disconnected upon issuance of a trip command, another command can be initiated using the breaker failure protection which operates the circuit-breaker, e.g. of an upstream (higher-level) protection relay. Breaker failure is detected if, after a trip command, current is still flowing in the faulted circuit. As an option, it is possible to make use of the circuit-breaker position indication.

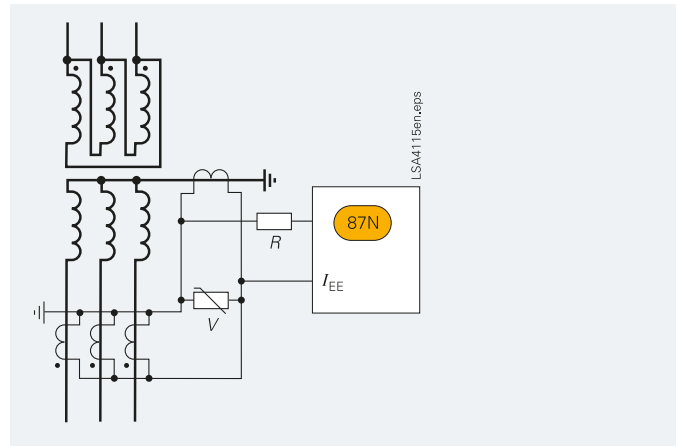


Fig. 5/27 High-impedance restricted ground-fault protection

### High-impedance restricted ground-fault protection (ANSI 87N)

The high-impedance measurement principle is an uncomplicated and sensitive method for detecting ground faults, especially on transformers. It can also be applied to motors, generators and reactors when these are operated on an grounded network.

When the high-impedance measurement principle is applied, all current transformers in the protected area are connected in parallel and operated on one common resistor of relatively high  $R$  whose voltage is measured (see Fig. 5/27). In the case of 7SJ6 units, the voltage is measured by detecting the current through the (external) resistor  $R$  at the sensitive current measurement input  $I_{EE}$ . The varistor  $V$  serves to limit the voltage in the event of an internal fault. It cuts off the high momentary voltage spikes occurring at transformer saturation. At the same time, this results in smoothing of the voltage without any noteworthy reduction of the average value.

If no faults have occurred and in the event of external faults, the system is at equilibrium, and the voltage through the resistor is approximately zero. In the event of internal faults, an imbalance occurs which leads to a voltage and a current flow through the resistor  $R$ .

The current transformers must be of the same type and must at least offer a separate core for the high-impedance restricted ground-fault protection. They must in particular have the same transformation ratio and an approximately identical knee-point voltage. They should also demonstrate only minimal measuring errors.

### Flexible protection functions

The 7SJ62 units enable the user to easily add on up to 20 protective functions. To this end, parameter definitions are used to link a standard protection logic with any chosen characteristic quantity (measured or derived quantity) (Fig. 5/28). The standard logic consists of the usual protection elements such as the pickup message, the parameter-definable delay time, the TRIP command, a blocking possibility, etc. The mode of operation for current, voltage, power and power factor quantities can be three-phase or single-phase. Almost all quantities can be operated as greater than or less than stages. All stages operate with protection priority.

Protection stages/functions attainable on the basis of the available characteristic quantities:

Function	ANSI No.
$I >, I_{E} >$	50, 50N
$V <, V >, V_{E} >, dV/dt$	27, 59, 59R, 64
$3I_{0} >, I_{1} >, I_{2} >, I_{2}/I_{1}, 3V_{0} >, V_{1} >, V_{2} >$	50N, 46, 59N, 47
$P >, Q >$	32
$\cos \varphi$ (p.f.) $>$	55
$f >$	810, 81U
$df/dt >$	81R

For example, the following can be implemented:

- Reverse power protection (ANSI 32R)
- Rate-of-frequency-change protection (ANSI 81R)

### Undervoltage-controlled reactive power protection (ANSI 27/Q)

The undervoltage-controlled reactive power protection protects the system for mains decoupling purposes. To prevent a voltage collapse in energy systems, the generating side, e.g. a generator, must be equipped with voltage and frequency protection devices. An undervoltage-controlled reactive power protection is required at the supply system connection point. It detects critical power system situations and ensures that the power generation facility is disconnected from the mains. Furthermore, it ensures that reconnection only takes place under stable power system conditions. The associated criteria can be parameterized.

### Synchro-check (ANSI 25)

In case of switching ON the circuit-breaker, the units can check whether the two subnetworks are synchronized. Voltage-, frequency- and phase-angle-differences are being checked to determine whether synchronous conditions are existent.

### Auto-reclosure (ANSI 79)

Multiple reclosures can be defined by the user and lockout will occur if a fault is present after the last reclosure. The following functions are possible:

- 3-pole ARC for all types of faults
- Separate settings for phase and ground faults
- Multiple ARC, one rapid auto-reclosure (RAR) and up to nine delayed auto-reclosures (DAR)

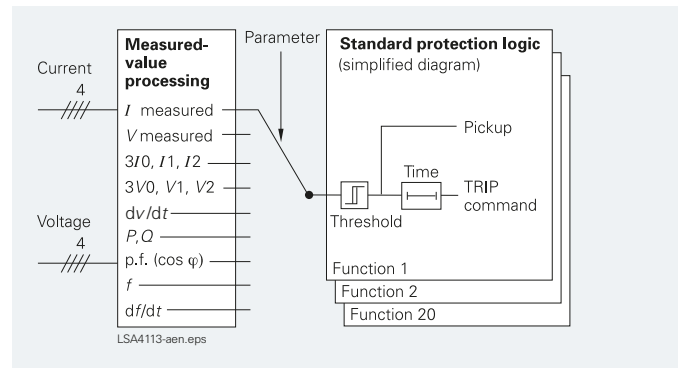


Fig. 5/28 Flexible protection functions

- Starting of the ARC depends on the trip command selection (e.g. 46, 50, 51, 67)
- Blocking option of the ARC via binary inputs
- ARC can be initiated externally or via CFC
- The directional and non-directional elements can either be blocked or operated non-delayed depending on the auto-reclosure cycle
- Dynamic setting change of the directional and non-directional elements can be activated depending on the ready AR

### Thermal overload protection (ANSI 49)

For protecting cables and transformers, an overload protection with an integrated pre-warning element for temperature and current can be applied. The temperature is calculated using a thermal homogeneous-body model (according to IEC 60255-8), which takes account both of the energy entering the equipment and the energy losses. The calculated temperature is constantly adjusted accordingly. Thus, account is taken of the previous load and the load fluctuations.

For thermal protection of motors (especially the stator) a further time constant can be set so that the thermal ratios can be detected correctly while the motor is rotating and when it is stopped. The ambient temperature or the temperature of the coolant can be detected serially via an external temperature monitoring box (resistance-temperature detector box, also called RTD-box). The thermal replica of the overload function is automatically adapted to the ambient conditions. If there is no RTD-box it is assumed that the ambient temperatures are constant.

### Settable dropout delay times

If the devices are used in parallel with electromechanical relays in networks with intermittent faults, the long dropout times of the electromechanical devices (several hundred milliseconds) can lead to problems in terms of time grading. Clean time grading is only possible if the dropout time is approximately the same. This is why the parameter of dropout times can be defined for certain functions such as time-over-current protection, ground short-circuit and phase-balance current protection.

## Protection functions

### ■ Motor protection

#### Restart inhibit (ANSI 66/86)

If a motor is started up too many times in succession, the rotor can be subject to thermal overload, especially the upper edges of the bars. The rotor temperature is calculated from the stator current. The reclosing lockout only permits start-up of the motor if the rotor has sufficient thermal reserves for a complete start-up (see Fig. 5/29).

#### Emergency start-up

This function disables the reclosing lockout via a binary input by storing the state of the thermal replica as long as the binary input is active. It is also possible to reset the thermal replica to zero.

#### Temperature monitoring (ANSI 38)

Up to two temperature monitoring boxes with a total of 12 measuring sensors can be used for temperature monitoring and detection by the protection relay. The thermal status of motors, generators and transformers can be monitored with this device. Additionally, the temperature of the bearings of rotating machines are monitored for limit value violation. The temperatures are being measured with the help of temperature detectors at various locations of the device to be protected. This data is transmitted to the protection relay via one or two temperature monitoring boxes (see "Accessories", page 5/115).

#### Starting time supervision (ANSI 48/14)

Starting time supervision protects the motor against long unwanted start-ups that might occur in the event of excessive load torque or excessive voltage drops within the motor, or if the rotor is locked. Rotor temperature is calculated from measured stator current. The tripping time is calculated according to the following equation:

for  $I > I_{\text{MOTOR START}}$

$$t = \left( \frac{I_A}{I} \right)^2 \cdot T_A$$

$I$  = Actual current flowing

$I_{\text{MOTOR START}}$  = Pickup current to detect a motor start

$t$  = Tripping time

$I_A$  = Rated motor starting current

$T_A$  = Tripping time at rated motor starting current  
(2 times, for warm and cold motor)

The characteristic (equation) can be adapted optimally to the state of the motor by applying different tripping times  $T_A$  in dependence of either cold or warm motor state. For differentiation of the motor state the thermal model of the rotor is applied.

If the trip time is rated according to the above formula, even a prolonged start-up and reduced voltage (and reduced start-up current) will be evaluated correctly. The tripping time is inverse (current dependent).

A binary signal is set by a speed sensor to detect a blocked rotor. An instantaneous tripping is effected.

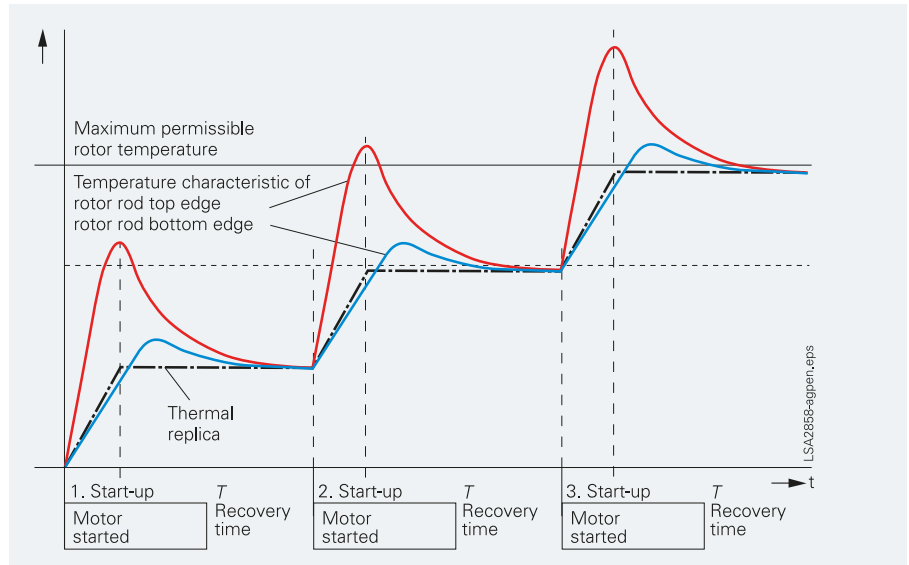


Fig. 5/29

#### Load jam protection (ANSI 51M)

Sudden high loads can cause slowing down and blocking of the motor and mechanical damages. The rise of current due to a load jam is being monitored by this function (alarm and tripping).

The overload protection function is too slow and therefore not suitable under these circumstances.

#### Phase-balance current protection (ANSI 46) (Negative-sequence protection)

The negative-sequence / phase-balance current protection detects a phase failure or load unbalance due to network asymmetry and protects the rotor from impermissible temperature rise.

#### Undercurrent monitoring (ANSI 37)

With this function, a sudden drop in current, which can occur due to a reduced motor load, is detected. This may be due to shaft breakage, no-load operation of pumps or fan failure.

#### Motor statistics

Essential information on start-up of the motor (duration, current, voltage) and general information on number of starts, total operating time, total down time, etc. are saved as statistics in the device.

### ■ Voltage protection

#### Overvoltage protection (ANSI 59)

The two-element overvoltage protection detects unwanted network and machine overvoltage conditions. The function can operate either with phase-to-phase, phase-to-ground, positive phase-sequence or negative phase-sequence system voltage. Three-phase and single-phase connections are possible.

#### Undervoltage protection (ANSI 27)

The two-element undervoltage protection provides protection against dangerous voltage drops (especially for electric machines). Applications include the isolation of generators or motors from the network to avoid undesired operating states and a possible loss of stability. Proper operating conditions of electrical machines are best evaluated with the positive-sequence quantities. The protection function is active over a



wide frequency range (45 to 55, 55 to 65 Hz)<sup>1)</sup>. Even when falling below this frequency range the function continues to work, however, with a greater tolerance band.

The function can operate either with phase-to-phase, phase-to-ground or positive phase-sequence voltage and can be monitored with a current criterion. Three-phase and single-phase connections are possible.

### Frequency protection (ANSI 81O/U)

Frequency protection can be used for over-frequency and under-frequency protection. Electric machines and parts of the system are protected from unwanted speed deviations. Unwanted frequency changes in the network can be detected and the load can be removed at a specified frequency setting.

Frequency protection can be used over a wide frequency range (40 to 60, 50 to 70 Hz)<sup>1)</sup>. There are four elements (selectable as overfrequency or underfrequency) and each element can be delayed separately. Blocking of the frequency protection can be performed if using a binary input or by using an undervoltage element.

### Fault locator (ANSI 21FL)

The integrated fault locator calculates the fault impedance and the distance-to-fault. The results are displayed in  $\Omega$ , kilometers (miles) and in percent of the line length.

### Circuit-breaker wear monitoring

Methods for determining circuit-breaker contact wear or the remaining service life of a circuit-breaker (CB) allow CB maintenance intervals to be aligned to their actual degree of wear. The benefit lies in reduced maintenance costs.

There is no mathematically exact method of calculating the wear or the remaining service life of circuit-breakers that takes into account the arc-chamber's physical conditions when the CB opens. This is why various methods of determining CB wear have evolved which reflect the different operator philosophies. To do justice to these, the devices offer several methods:

- $\Sigma I$
- $\Sigma I^x$ , with  $x = 1 \dots 3$
- $\Sigma i^2t$

The devices additionally offer a new method for determining the remaining service life:

- Two-point method

The CB manufacturers double-logarithmic switching cycle diagram (see Fig. 5/30) and the breaking current at the time of contact opening serve as the basis for this method. After CB opening, the two-point method calculates the number of still possible switching cycles. To this end, the two points P1 and P2 only have to be set on the device. These are specified in the CB's technical data.

All of these methods are phase-selective and a limit value can be set in order to obtain an alarm if the actual value falls below or exceeds the limit value during determination of the remaining service life.

### Customized functions (ANSI 32, 51V, 55, etc.)

Additional functions, which are not time critical, can be implemented via the CFC using measured values. Typical functions include reverse power, voltage controlled overcurrent, phase angle detection, and zero-sequence voltage detection.

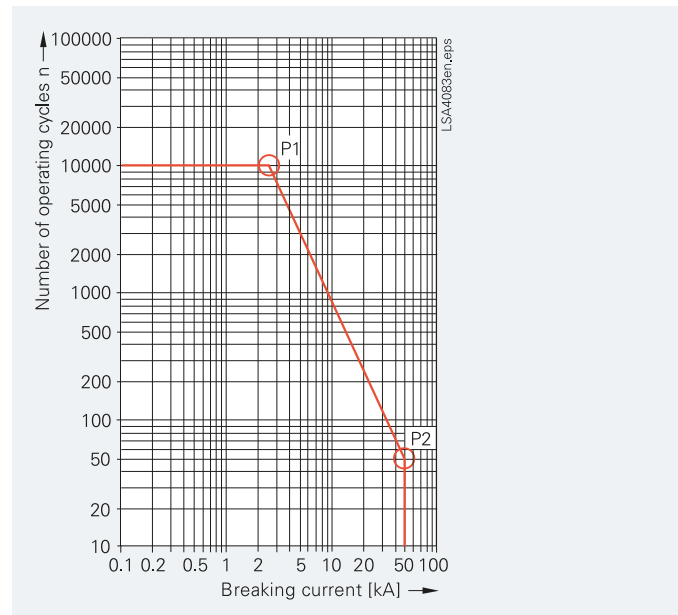


Fig. 5/30 CB switching cycle diagram

### Commissioning

Commissioning could hardly be easier and is fully supported by DIGSI 4. The status of the binary inputs can be read individually and the state of the binary outputs can be set individually. The operation of switching elements (circuit-breakers, disconnect devices) can be checked using the switching functions of the bay controller. The analog measured values are represented as wide-ranging operational measured values. To prevent transmission of information to the control center during maintenance, the bay controller communications can be disabled to prevent unnecessary data from being transmitted. During commissioning, all indications with test marking for test purposes can be connected to a control and protection system.

### Test operation

During commissioning, all indications can be passed to an automatic control system for test purposes.

### Control and automatic functions

#### Control

In addition to the protection functions, the SIPROTEC 4 units also support all control and monitoring functions that are required for operating medium-voltage or high-voltage substations.

The main application is reliable control of switching and other processes.

The status of primary equipment or auxiliary devices can be obtained from auxiliary contacts and communicated to the 7SJ62 via binary inputs. Therefore it is possible to detect and indicate both the OPEN and CLOSED position or a fault or intermediate circuit-breaker or auxiliary contact position.

The switchgear or circuit-breaker can be controlled via:

- integrated operator panel
- binary inputs
- substation control and protection system
- DIGSI 4

1) The 45 to 55, 55 to 65 Hz range is available for  $f_N = 50/60$  Hz.

# Overcurrent Protection / 7SJ62

## Functions

### Automation/user-defined logic

With integrated logic, the user can set, via a graphic interface (CFC), specific functions for the automation of switchgear or substation. Functions are activated via function keys, binary input or via communication interface.

### Switching authority

Switching authority is determined according to parameters and communication.

If a source is set to "LOCAL", only local switching operations are possible. The following sequence of switching authority is laid down: "LOCAL"; DIGSI PC program, "REMOTE".

### Command processing

All the functionality of command processing is offered. This includes the processing of single and double commands with or without feedback, sophisticated monitoring of the control hardware and software, checking of the external process, control actions using functions such as runtime monitoring and automatic command termination after output. Here are some typical applications:

- Single and double commands using 1, 1 plus 1 common or 2 trip contacts
- User-definable bay interlocks
- Operating sequences combining several switching operations such as control of circuit-breakers, disconnectors and grounding switches
- Triggering of switching operations, indications or alarm by combination with existing information

### Assignment of feedback to command

The positions of the circuit-breaker or switching devices and transformer taps are acquired by feedback. These indication inputs are logically assigned to the corresponding command outputs. The unit can therefore distinguish whether the indication change is a consequence of switching operation or whether it is a spontaneous change of state.

### Chatter disable

Chatter disable feature evaluates whether, in a configured period of time, the number of status changes of indication input exceeds a specified figure. If exceeded, the indication input is blocked for a certain period, so that the event list will not record excessive operations.

### Indication filtering and delay

Binary indications can be filtered or delayed.

Filtering serves to suppress brief changes in potential at the indication input. The indication is passed on only if the indication voltage is still present after a set period of time. In the event of indication delay, there is a wait for a preset time. The information is passed on only if the indication voltage is still present after this time.

### Indication derivation

A further indication (or a command) can be derived from an existing indication. Group indications can also be formed. The volume of information to the system interface can thus be reduced and restricted to the most important signals.



Fig. 5/31 NXAIR panel (air-insulated)

### Switchgear cubicles for high/medium voltage

All units are designed specifically to meet the requirements of high/medium-voltage applications.

In general, no separate measuring instruments (e.g., for current, voltage, frequency, ...) or additional control components are necessary.

### Measured values

The r.m.s. values are calculated from the acquired current and voltage along with the power factor, frequency, active and reactive power. The following functions are available for measured value processing:

- Currents  $I_{L1}$ ,  $I_{L2}$ ,  $I_{L3}$ ,  $I_E$ ,  $I_{EE}$  (67Ns)
- Voltages  $V_{L1}$ ,  $V_{L2}$ ,  $V_{L3}$ ,  $V_{L1L2}$ ,  $V_{L2L3}$ ,  $V_{L3L1}$
- Symmetrical components  $I_1$ ,  $I_2$ ,  $3I_0$ ;  $V_1$ ,  $V_2$ ,  $V_0$
- Power Watts, Vars,  $VA/P$ ,  $Q$ ,  $S$  ( $P$ ,  $Q$ : total and phase selective)
- Power factor ( $\cos \varphi$ ), (total and phase selective)
- Frequency
- Energy  $\pm$  kWh,  $\pm$  kVarh, forward and reverse power flow
- Mean as well as minimum and maximum current and voltage values
- Operating hours counter
- Mean operating temperature of overload function
- Limit value monitoring  
Limit values are monitored using programmable logic in the CFC. Commands can be derived from this limit value indication.
- Zero suppression  
In a certain range of very low measured values, the value is set to zero to suppress interference.

### Communication

In terms of communication, the units offer substantial flexibility in the context of connection to industrial and power automation standards. Communication can be extended or added on thanks to modules for retrofitting on which the common protocols run. Therefore, also in the future it will be possible to optimally integrate units into the changing communication infrastructure, for example in Ethernet networks (which will also be used increasingly in the power supply sector in the years to come).

#### Serial front interface

There is a serial RS232 interface on the front of all the units. All of the unit's functions can be set on a PC by means of the DIGSI 4 protection operation program. Commissioning tools and fault analysis are also built into the program and are available through this interface.

#### Rear-mounted interfaces<sup>1)</sup>

A number of communication modules suitable for various applications can be fitted in the rear of the flush-mounting housing. In the flush-mounting housing, the modules can be easily replaced by the user. The interface modules support the following applications:

- Time synchronization interface  
All units feature a permanently integrated electrical time synchronization interface. It can be used to feed timing telegrams in IRIG-B or DCF77 format into the units via time synchronization receivers.
- System interface  
Communication with a central control system takes place through this interface. Radial or ring type station bus topologies can be configured depending on the chosen interface. Furthermore, the units can exchange data through this interface via Ethernet and IEC 61850 protocol and can also be operated by DIGSI.
- Service interface  
The service interface was conceived for remote access to a number of protection units via DIGSI. On all units, it can be an electrical RS232/RS485 or an optical interface. For special applications, a maximum of two temperature monitoring boxes (RTD-box) can be connected to this interface as an alternative.

#### System interface protocols (retrofittable)

##### IEC 61850 protocol

The Ethernet-based IEC 61850 protocol is the worldwide standard for protection and control systems used by power supply corporations. Siemens was the first manufacturer to support this standard. By means of this protocol, information can also be exchanged directly between bay units so as to set up simple masterless systems for bay and system interlocking. Access to the units via the Ethernet bus is also possible with DIGSI.

##### IEC 60870-5-103 protocol

The IEC 60870-5-103 protocol is an international standard for the transmission of protective data and fault recordings. All messages from the unit and also control commands can be transferred by means of published, Siemens-specific extensions to the protocol.

1) For units in panel surface-mounting housings please refer to note on page 5/114.

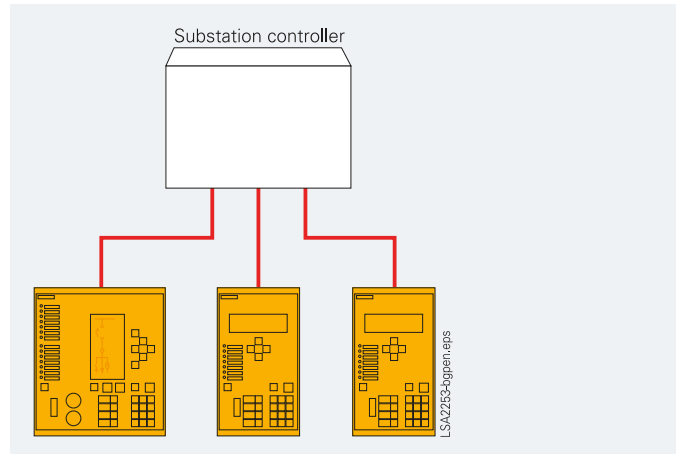


Fig. 5/32 IEC 60870-5-103: Radial fiber-optic connection

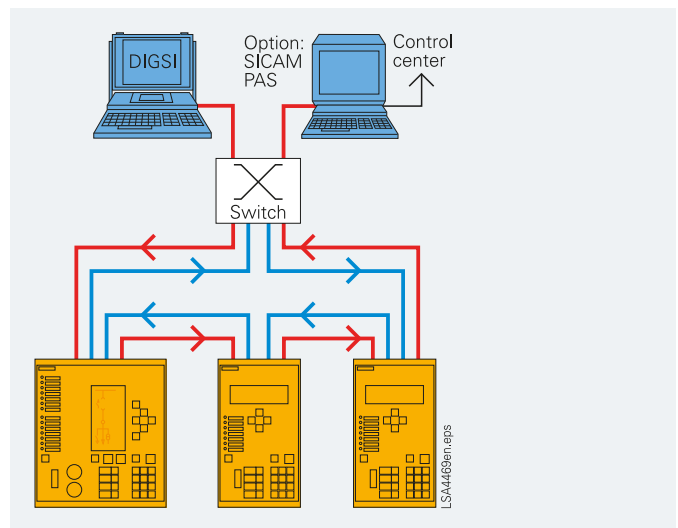


Fig. 5/33 Bus structure for station bus with Ethernet and IEC 61850, fiber-optic ring

Redundant solutions are also possible. Optionally it is possible to read out and alter individual parameters (only possible with the redundant module).

#### PROFIBUS DP protocol

PROFIBUS DP is the most widespread protocol in industrial automation. Via PROFIBUS DP, SIPROTEC units make their information available to a SIMATIC controller or, in the control direction, receive commands from a central SIMATIC. Measured values can also be transferred.

#### MODBUS RTU protocol

This uncomplicated, serial protocol is mainly used in industry and by power supply corporations, and is supported by a number of unit manufacturers. SIPROTEC units function as MODBUS slaves, making their information available to a master or receiving information from it. A time-stamped event list is available.

# Overcurrent Protection / 7SJ62

## Communication

### PROFINET

PROFINET is the ethernet-based successor of Profi bus DP and is supported in the variant PROFINET IO. The protocol which is used in industry together with the SIMATIC systems control is realized on the optical and electrical Plus ethernet modules which are delivered since November 2012. All network redundancy procedures which are available for the ethernet modules, such as RSTP, PRP or HSR, are also available for PROFINET. The time synchronization is made via SNTP. The network monitoring is possible via SNMP V2 where special MIB files exist for PROFINET. The LLDP protocol of the device also supports the monitoring of the network topology. Single-point indications, double-point indications, measured and metered values can be transmitted cyclically in the monitoring direction via the protocol and can be selected by the user with DIGSI 4. Important events are also transmitted spontaneously via configurable process alarms. Switching commands can be executed by the system control via the device in the controlling direction. The PROFINET implementation is certified. The device also supports the IEC 61850 protocol as a server on the same ethernet module in addition to the PROFINET protocol. Client server connections are possible for the intercommunication between devices, e.g. for transmitting fault records and GOOSE messages.

### DNP 3.0 protocol

Power utilities use the serial DNP 3.0 (Distributed Network Protocol) for the station and network control levels. SIPROTEC units function as DNP slaves, supplying their information to a master system or receiving information from it.

### DNP3 TCP

The ethernet-based TCP variant of the DNP3 protocol is supported with the electrical and optical ethernet module. Two DNP3 TCP clients are supported. Redundant ring structures can be realized for DNP3 TCP with the help of the integrated switch in the module. For instance, a redundant optical ethernet ring can be constructed. Single-point indications, double-point indications, measured and metered values can be configured with DIGSI 4 and are transmitted to the DNPi client. Switching commands can be executed in the controlling direction. Fault records of the device are stored in the binary Comtrade format and can be retrieved via the DNP 3 file transfer. The time synchronization is performed via the DNPi client or SNTP. The device can also be integrated into a network monitoring system via the SNMP V2 protocol. Parallel to the DNP3 TCP protocol the IEC 61850 protocol (the device works as a server) and the GOOSE messages of the IEC 61850 are available for the intercommunication between devices.

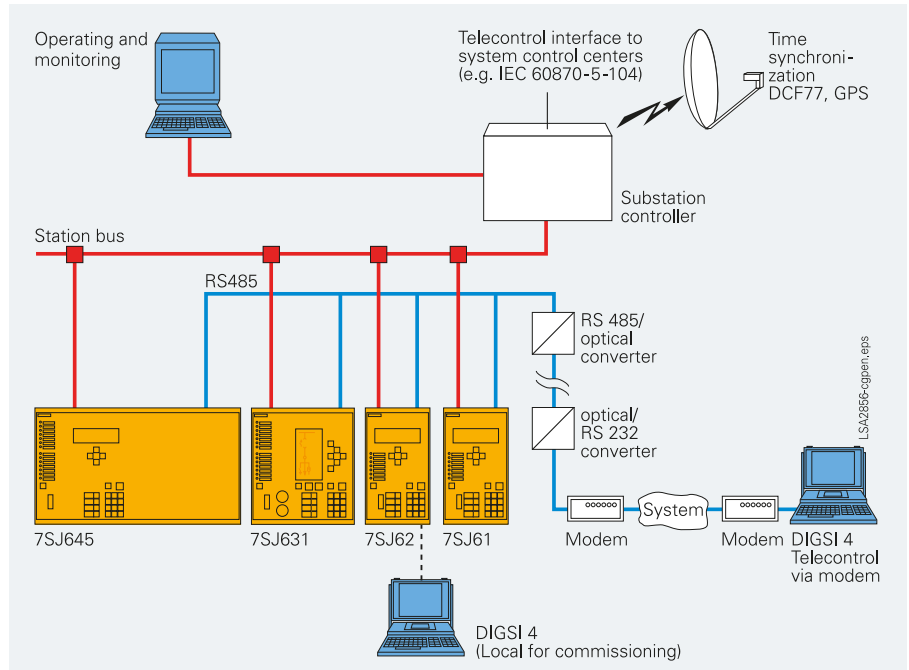


Fig. 5/34 System solution/communication

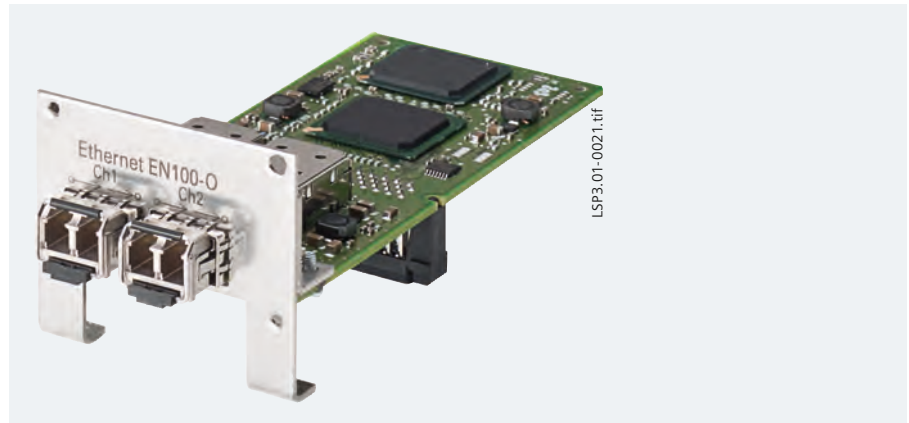


Fig. 5/35 Optical Ethernet communication module for IEC 61850 with integrated Ethernet-switch

### System solutions for protection and station control

Together with the SICAM power automation system, SIPROTEC 4 can be used with PROFIBUS DP. Over the low-cost electrical RS485 bus, or interference-free via the optical double ring, the units exchange information with the control system.

Units featuring IEC 60870-5-103 interfaces can be connected to SICAM in parallel via the RS485 bus or radially by fiber-optic link. Through this interface, the system is open for the connection of units of other manufacturers (see Fig. 5/32).

Because of the standardized interfaces, SIPROTEC units can also be integrated into systems of other manufacturers or in SIMATIC. Electrical RS485 or optical interfaces are available. The optimum physical data transfer medium can be chosen thanks to optoelectrical converters. Thus, the RS485 bus allows low-cost wiring

in the cubicles and an interference-free optical connection to the master can be established.

For IEC 61850, an interoperable system solution is offered with SICAM PAS. Via the 100 Mbits/s Ethernet bus, the units are linked with PAS electrically or optically to the station PC. The interface is standardized, thus also enabling direct connection of units of other manufacturers to the Ethernet bus. With IEC 61850, however, the units can also be used in other manufacturers' systems (see Fig. 5/33).

### Typical connections

#### ■ Connection of current and voltage transformers

##### Standard connection

For grounded networks, the ground current is obtained from the phase currents by the residual current circuit.

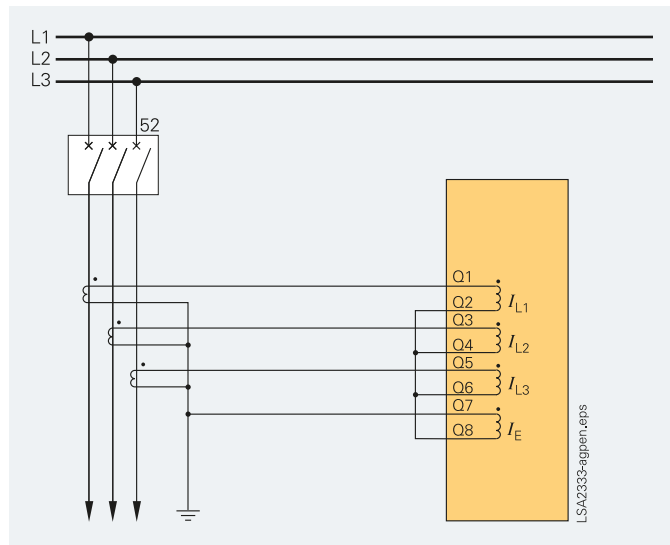


Fig. 5/36 Residual current circuit without directional element

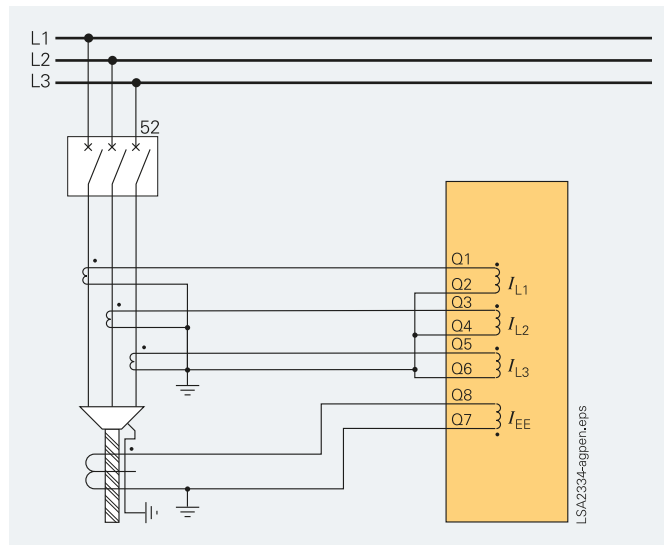


Fig. 5/37 Sensitive ground-current detection without directional element

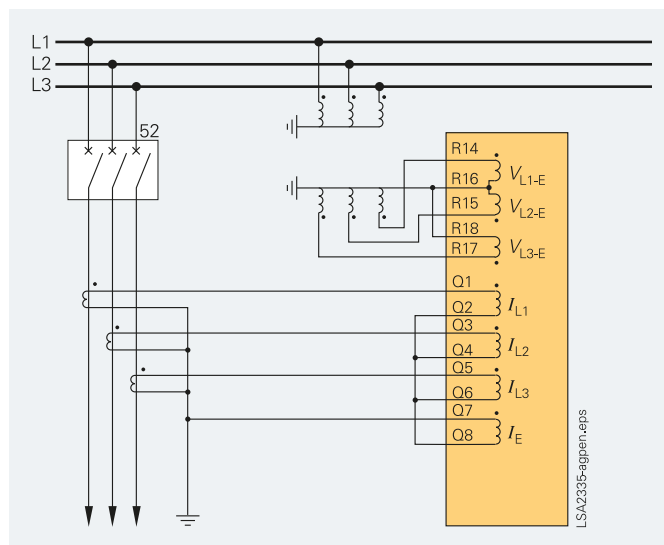


Fig. 5/38 Residual current circuit with directional element

# Overcurrent Protection / 7SJ62

## Typical connections

### Connection for compensated networks

The figure shows the connection of two phase-to-ground voltages and the  $V_E$  voltage of the open delta winding and a phase-balance neutral current transformer for the ground current. This connection maintains maximum precision for directional ground-fault detection and must be used in compensated networks. Fig. 5/39 shows sensitive directional ground-fault detection.

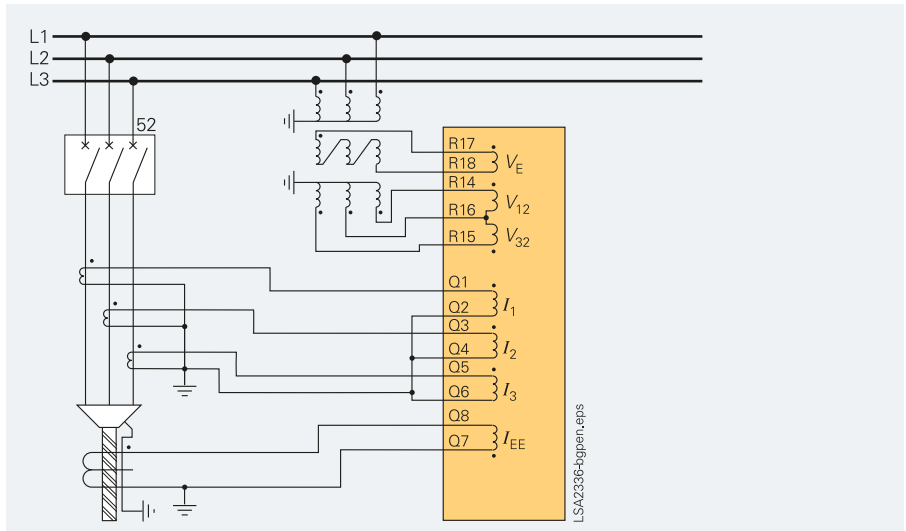


Fig. 5/39 Sensitive directional ground-fault detection with directional element for phases

### Connection for isolated-neutral or compensated networks only

If directional ground-fault protection is not used, the connection can be made with only two phase current transformers. Directional phase short-circuit protection can be achieved by using only two primary transformers.

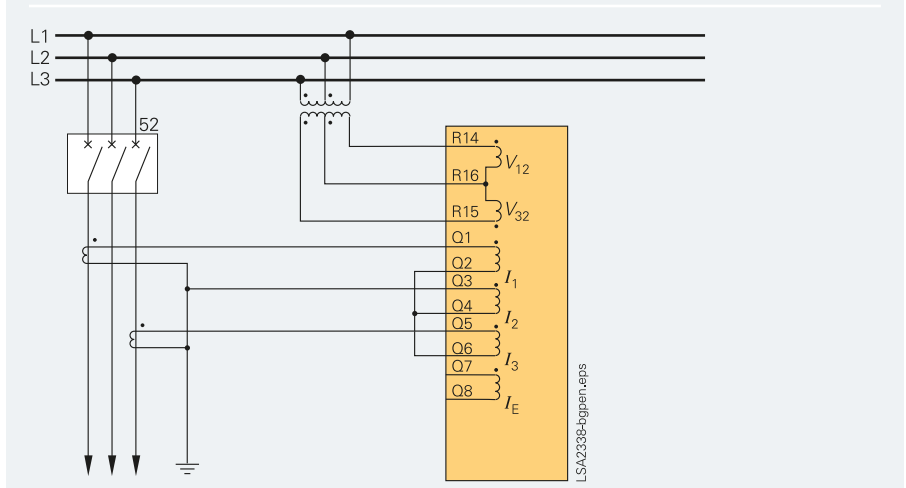


Fig. 5/40 Isolated-neutral or compensated networks

### Connection for the synchro-check function

The 3-phase system is connected as reference voltage, i. e. the outgoing voltages as well as a single-phase voltage, in this case a busbar voltage, that has to be checked for synchronism.

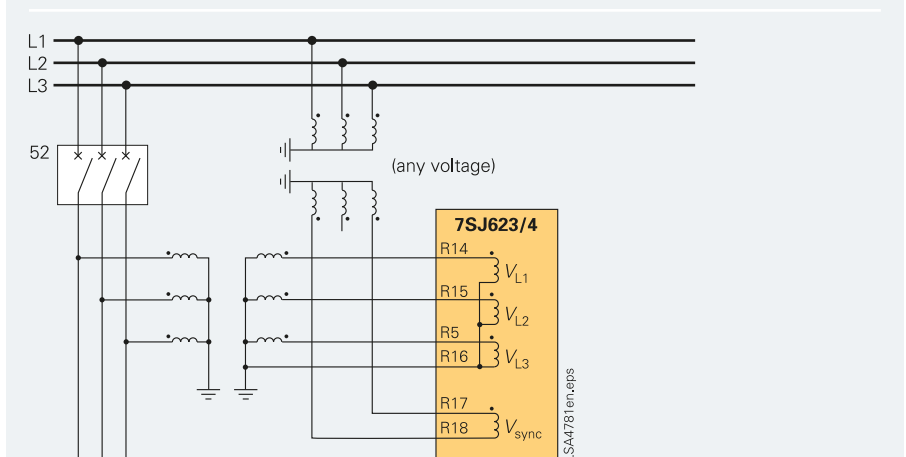


Fig. 5/41 Measuring of the busbar voltage and the outgoing feeder voltage for the synchro-check

Overview of connection types			
Type of network	Function	Current connection	Voltage connection
(Low-resistance) grounded network	Overcurrent protection phase/ground non-directional	Residual circuit, with 3 phase-current transformers required, phase-balance neutral current transformer possible	–
(Low-resistance) grounded networks	Sensitive ground-fault protection	Phase-balance neutral current transformers required	–
Isolated or compensated networks	Overcurrent protection phases non-directional	Residual circuit, with 3 or 2 phase current transformers possible	–
(Low-resistance) grounded networks	Overcurrent protection phases directional	Residual circuit, with 3 phase-current transformers possible	Phase-to-ground connection or phase-to-phase connection
Isolated or compensated networks	Overcurrent protection phases directional	Residual circuit, with 3 or 2 phase-current transformers possible	Phase-to-ground connection or phase-to-phase connection
(Low-resistance) grounded networks	Overcurrent protection ground directional	Residual circuit, with 3 phase-current transformers required, phase-balance neutral current transformers possible	Phase-to-ground connection required
Isolated networks	Sensitive ground-fault protection	Residual circuit, if ground current $> 0.05 I_N$ on secondary side, otherwise phase-balance neutral current transformers required	3 times phase-to-ground connection or phase-to-ground connection with open delta winding
Compensated networks	Sensitive ground-fault protection $\cos \varphi$ measurement	Phase-balance neutral current transformers required	Phase-to-ground connection with open delta winding required

### Typical applications

#### ■ Connection of circuit-breaker

#### Undervoltage releases

Undervoltage releases are used for automatic tripping of high-voltage motors.

Example:

DC supply voltage of control system fails and manual electric tripping is no longer possible.

Automatic tripping takes place when voltage across the coil drops below the trip limit. In Fig. 5/42, tripping occurs due to failure of DC supply voltage, by automatic opening of the live status contact upon failure of the protection unit or by short-circuiting the trip coil in event of network fault.

In Fig. 5/43 tripping is by failure of auxiliary voltage and by interruption of tripping circuit in the event of network failure. Upon failure of the protection unit, the tripping circuit is also interrupted, since contact held by internal logic drops back into open position.

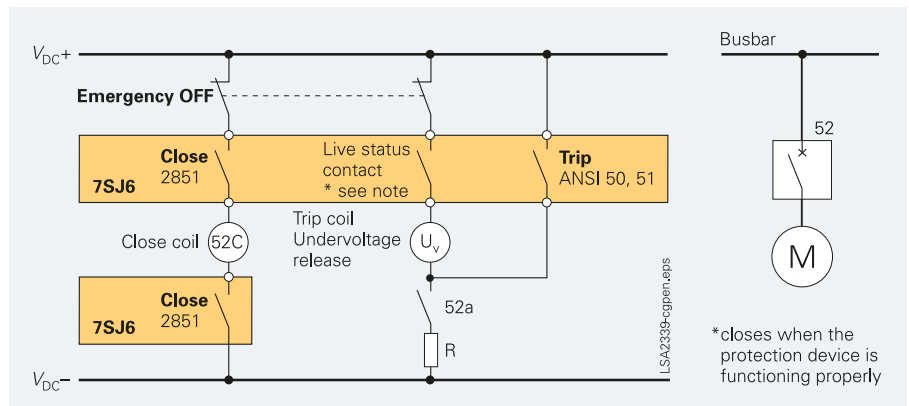


Fig. 5/42 Undervoltage release with make contact (50, 51)

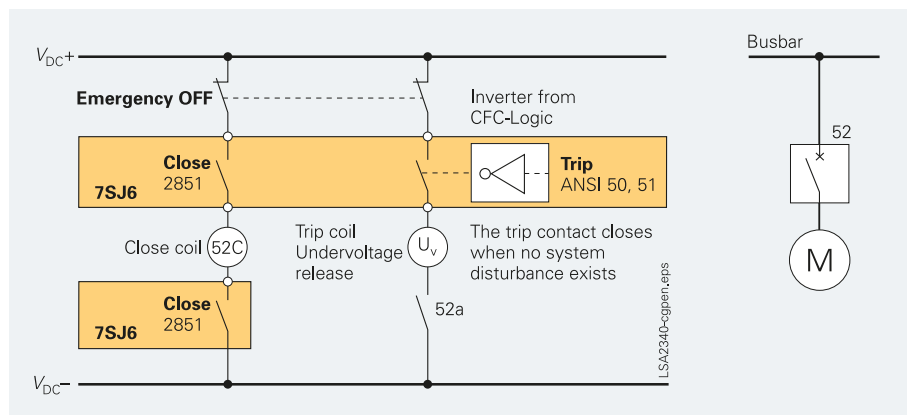


Fig. 5/43 Undervoltage trip with locking contact (trip signal 50 is inverted)

# Overcurrent Protection / 7SJ62

## Typical applications

### Trip circuit supervision (ANSI 74TC)

One or two binary inputs can be used for monitoring the circuit-breaker trip coil including its incoming cables. An alarm signal occurs whenever the circuit is interrupted.

### Lockout (ANSI 86)

All binary outputs can be stored like LEDs and reset using the LED reset key. The lockout state is also stored in the event of supply voltage failure. Reclosure can only occur after the lockout state is reset.

### Reverse-power protection for dual supply (ANSI 32R)

If power is fed to a busbar through two parallel infeeds, then in the event of any fault on one of the infeeds it should be selectively interrupted. This ensures a continued supply to the busbar through the remaining infeed. For this purpose, directional devices are needed which detect a short-circuit current or a power flow from the busbar in the direction of the infeed. The directional overcurrent protection is usually set via the load current. It cannot be used to deactivate low-current faults. Reverse-power protection can be set far below the rated power. This ensures that it also detects power feedback into the line in the event of low-current faults with levels far below the load current.

Reverse-power protection is performed via the "flexible protection functions" of the 7SJ62.

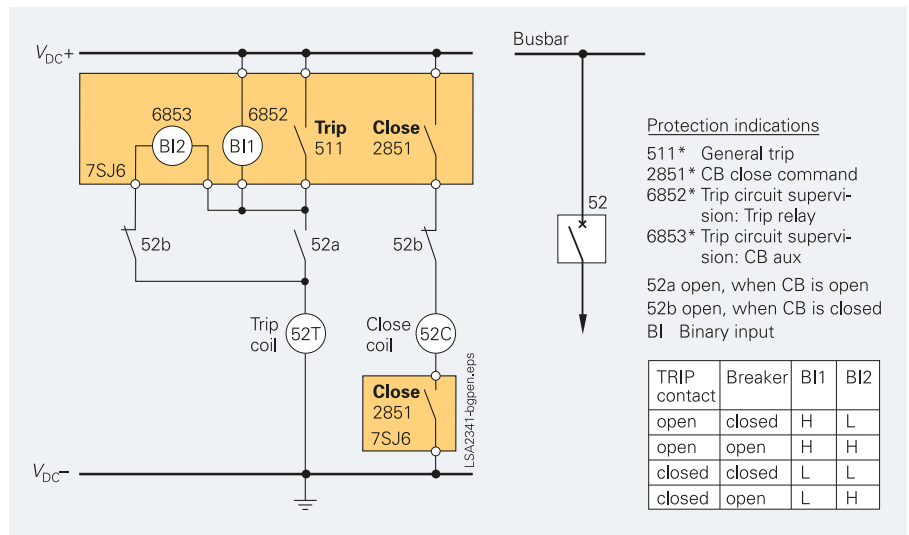


Fig. 5/44 Trip circuit supervision with 2 binary inputs

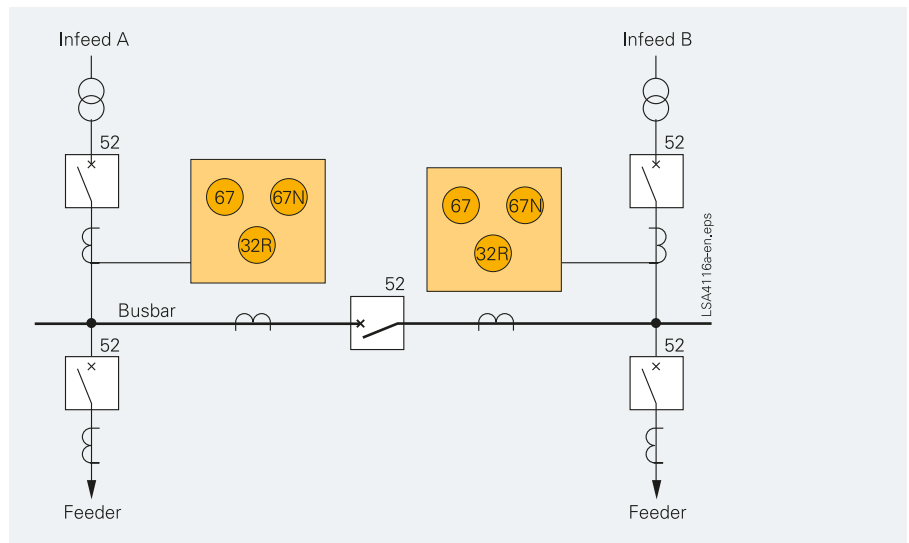


Fig. 5/45 Reverse-power protection for dual supply



General unit data	
<i>Measuring circuits</i>	
System frequency	50 / 60 Hz (settable)
<i>Current transformer</i>	
Rated current $I_{nom}$	1 or 5 A (settable)
Option: sensitive ground-fault CT	$I_{EE} < 1.6$ A
Power consumption	
at $I_{nom} = 1$ A	Approx. 0.05 VA per phase
at $I_{nom} = 5$ A	Approx. 0.3 VA per phase
for sensitive ground-fault CT at 1 A	Approx. 0.05 VA
Overload capability	
Thermal (effective)	500 A for 1 s 150 A for 10 s 20 A continuous
Dynamic (impulse current)	$250 \times I_{nom}$ (half cycle)
Overload capability if equipped with sensitive ground-fault CT	
Thermal (effective)	300 A for 1 s 100 A for 10 s 15 A continuous
Dynamic (impulse current)	750 A (half cycle)
<i>Voltage transformer</i>	
Type	7SJ621, 7SJ623, 7SJ625 7SJ622, 7SJ624, 7SJ626
Number	3 4 4
Rated voltage $V_{nom}$	100 V to 225 V
Measuring range	0 V to 170 V
Power consumption at $V_{nom} = 100$ V	< 0.3 VA per phase
Overload capability in voltage path (phase-neutral voltage)	
Thermal (effective)	230 V continuous
<i>Auxiliary voltage</i>	
Rated auxiliary voltage Vaux	DC 24/48 V 60/125 V 110/250 V AC 115/230 V
Permissible tolerance	DC 19-58 V 48-150 V 88-300 V AC 92-138 V 184-265 V
Ripple voltage, peak-to-peak	$\leq 12$ %
Power consumption	
Quiescent	Approx. 4 W
Energized	Approx. 7 W
Backup time during loss/short circuit of auxiliary voltage	$\geq 50$ ms at $V \geq$ DC 110 V $\geq 20$ ms at $V \geq$ DC 24 V $\geq 200$ ms at 115 V/AC 230 V
<i>Binary inputs/indication inputs</i>	
Type	7SJ621, 7SJ623, 7SJ625, 7SJ622, 7SJ624, 7SJ626
Number	8 11
Voltage range	DC 24-250 V
Pickup threshold modifiable by plug-in jumpers	
Pickup threshold	DC 19 V
For rated control voltage	24/48/60/110/125 V 110/125/DC 220/250 V
Response time/drop-out time	Approx. 3.5
Power consumption energized	1.8 mA (independent of operating voltage)

Binary outputs/command outputs	
Type	7SJ621, 7SJ622 7SJ623, 7SJ624 7SJ625, 7SJ626
Command/indication relay	8 6
Contacts per command/indication relay	1 NO / form A (Two contacts changeable to NC/form B, via jumpers)
Live status contact	1 NO / NC (jumper) / form A/B
Switching capacity	
Make	1000 W / VA
Break	30 W / VA / 40 W resistive / 25 W at $L/R \leq 50$ ms $\leq$ DC 250 V
Switching voltage	5 A continuous,
Permissible current	30 A for 0.5 s making current, 2000 switching cycles

Electrical tests	
<i>Specification</i>	
Standards	IEC 60255 ANSI C37.90, C37.90.1, C37.90.2, UL508

Insulation tests	
Standards	IEC 60255-5; ANSI/IEEE C37.90.0
Voltage test (100 % test) all circuits except for auxiliary voltage and RS485/RS232 and time synchronization	2.5 kV (r.m.s. value), 50/60 Hz
Auxiliary voltage	DC 3.5 kV
Communication ports and time synchronization	AC 500 V
Impulse voltage test (type test) all circuits, except communication ports and time synchronization, class III	5 kV (peak value); 1.2/50 $\mu$ s; 0.5 J 3 positive and 3 negative impulses at intervals of 5 s

EMC tests for interference immunity; type tests	
Standards	IEC 60255-6; IEC 60255-22 (product standard) EN 50082-2 (generic specification) DIN 57435 Part 303
High-frequency test IEC 60255-22-1, class III and VDE 0435 Part 303, class III	2.5 kV (peak value); 1 MHz; $\tau = 15$ ms; 400 surges per s; test duration 2 s
Electrostatic discharge IEC 60255-22-2 class IV and EN 61000-4-2, class IV	8 kV contact discharge; 15 kV air gap discharge; both polarities; 150 pF; $R_i = 330 \Omega$
Irradiation with radio-frequency field, non-modulated IEC 60255-22-3 (Report) class III	10 V/m; 27 to 500 MHz
Irradiation with radio-frequency field, amplitude-modulated IEC 61000-4-3; class III	10 V/m, 80 to 1000 MHz; AM 80 %; 1 kHz
Irradiation with radio-frequency field, pulse-modulated IEC 61000-4-3/ENV 50204; class III	10 V/m, 900 MHz; repetition rate 200 Hz, on duration 50 %
Fast transient interference/burst IEC 60255-22-4 and IEC 61000-4-4, class IV	4 kV; 5/50 ns; 5 kHz; burst length = 15 ms; repetition rate 300 ms; both polarities; $R_i = 50 \Omega$ ; test duration 1 min

# Overcurrent Protection / 7SJ62

## Technical data

5

### EMC tests for interference immunity; type tests (cont'd)

High-energy surge voltages (Surge) IEC 61000-4-5; class III Auxiliary voltage	From circuit to circuit: 2 kV; 12 Ω; 9 μF across contacts: 1 kV; 2 Ω; 18 μF
Binary inputs/outputs	From circuit to circuit: 2 kV; 42 Ω; 0.5 μF across contacts: 1 kV; 42 Ω; 0.5 μF
Line-conducted HF, amplitude-modulated IEC 61000-4-6, class III	10 V; 150 kHz to 80 MHz; AM 80 %; 1 kHz
Power frequency magnetic field IEC 61000-4-8, class IV IEC 60255-6	30 A/m; 50 Hz, continuous 300 A/m; 50 Hz, 3 s 0.5 mT, 50 Hz
Oscillatory surge withstand capability ANSI/IEEE C37.90.1	2.5 to 3 kV (peak value), 1 to 1.5 MHz damped wave; 50 surges per s; duration 2 s, $R_i = 150$ to 200 Ω
Fast transient surge withstand capability ANSI/IEEE C37.90.1	4 to 5 kV; 10/150 ns; 50 surges per s both polarities; duration 2 s, $R_i = 80$ Ω
Radiated electromagnetic interference ANSI/IEEE C37.90.2	35 V/m; 25 to 1000 MHz; amplitude and pulse-modulated
Damped wave IEC 60694 / IEC 61000-4-12	2.5 kV (peak value, polarity alternating) 100 kHz, 1 MHz, 10 and 50 MHz, $R_i = 200$ Ω

### EMC tests for interference emission; type tests

Standard	EN 50081-* (generic specification)
Conducted interferences only auxiliary voltage IEC/CISPR 22	150 kHz to 30 MHz Limit class B
Radio interference field strength IEC/CISPR 11	30 to 1000 MHz Limit class B
Units with a detached operator panel must be installed in a metal cubicle to maintain limit class B	

### Mechanical stress tests

#### Vibration, shock stress and seismic vibration

##### During operation

Standards	IEC 60255-21 and IEC 60068-2
Vibration IEC 60255-21-1, class 2 IEC 60068-2-6	Sinusoidal 10 to 60 Hz; ± 0.075 mm amplitude; 60 to 150 Hz; 1 g acceleration frequency sweep 1 octave/min 20 cycles in 3 perpendicular axes
Shock IEC 60255-21-2, class 1 IEC 60068-2-27	Semi-sinusoidal Acceleration 5 g, duration 11 ms; 3 shocks in both directions of 3 axes
Seismic vibration IEC 60255-21-3, class 1 IEC 60068-3-3	Sinusoidal 1 to 8 Hz: ± 3.5 mm amplitude (horizontal axis) 1 to 8 Hz: ± 1.5 mm amplitude (vertical axis) 8 to 35 Hz: 1 g acceleration (horizontal axis) 8 to 35 Hz: 0.5 g acceleration (vertical axis) Frequency sweep 1 octave/min 1 cycle in 3 perpendicular axe

### During transportation

Standards	IEC 60255-21 and IEC 60068-2
Vibration IEC 60255-21-1, class 2 IEC 60068-2-6	Sinusoidal 5 to 8 Hz: ± 7.5 mm amplitude; 8 to 150 Hz; 2 g acceleration, frequency sweep 1 octave/min 20 cycles in 3 perpendicular axes
Shock IEC 60255-21-2, Class 1 IEC 60068-2-27	Semi-sinusoidal Acceleration 15 g, duration 11 ms 3 shocks in both directions of 3 axes
Continuous shock IEC 60255-21-2, class 1 IEC 60068-2-29	Semi-sinusoidal Acceleration 10 g, duration 16 ms 1000 shocks in both directions of 3 axes

### Climatic stress tests

#### Temperatures

Type-tested acc. to IEC 60068-2-1 and -2, test Bd, for 16 h	-25 °C to +85 °C / -13 °F to +185 °F
Temporarily permissible operating temperature, tested for 96 h	-20 °C to +70 °C / -4 °F to -158 °F
Recommended permanent operating temperature acc. to IEC 60255-6 (Legibility of display may be impaired above +55 °C / +131 °F)	-5 °C to +55 °C / +25 °F to +131 °F
- Limiting temperature during permanent storage	-25 °C to +55 °C / -13 °F to +131 °F
- Limiting temperature during transport	-25 °C to +70 °C / -13 °F to +158 °F

#### Humidity

Permissible humidity It is recommended to arrange the units in such a way that they are not exposed to direct sunlight or pronounced temperature changes that could cause condensation.	Annual average 75 % relative humidity; on 56 days a year up to 95 % relative humidity; condensation not permissible!
--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------	----------------------------------------------------------------------------------------------------------------------

#### Unit design

Housing	7XP20
Dimensions	See dimension drawings, part 14
Weight	
Surface-mounting housing	4.5 kg
Flush-mounting housing	4.0 kg
Degree of protection acc. to EN 60529	
Surface-mounting housing	IP 51
Flush-mounting housing	Front: IP 51, rear: IP 20;
Operator safety	IP 2x with cover

Further information can be found in the current manual at:  
[www.siemens.com/siprotec](http://www.siemens.com/siprotec)







# Overcurrent Protection / 7SJ62

## Selection and ordering data

5

Description			Order No.	Order code
<b>7SJ62 multifunction protection relay</b>			<b>7SJ62</b> □ □ - □ □ □ □ □ □ - □ □ □ □	
Designation	ANSI No.	Description		
Basic version		Control		
	50/51	Overcurrent protection $I>$ , $I>>$ , $I>>>$ , $I_p$		
	50N/51N	Ground-fault protection $I_{E>}$ , $I_{E>>}$ , $I_{E>>>}$ , $I_{Ep}$		
	50N/51N	Insensitive ground-fault protection via IEE function: $I_{EE>}$ , $I_{EE>>}$ , $I_{EEp}$ <sup>1)</sup>		
	50/50N	Flexible protection functions (index quantities derived from current): Additional time-overcurrent protection, stages $I_{2>}$ , $I_{2>>>}$ , $I_{E>>>>}$		
	51 V	Voltage-dependent inverse-time overcurrent protection		
	49	Overload protection (with 2 time constants)		
	46	Phase balance current protection (negative-sequence protection)		
	37	Undercurrent monitoring		
	47	Phase sequence		
	59N/64	Displacement voltage		
	50BF	Breaker failure protection		
	74TC	Trip circuit supervision 4 setting groups, cold-load pickup Inrush blocking		
	86	Lockout		
Sens. ground-f. det. Motor IEF	67/67N	Direction determination for overcurrent, phases and ground		
Dir IEF V,P,f REF	67Ns	Directional sensitive ground-fault detection		
■	67Ns	Directional intermittent ground fault protection <sup>4)</sup>		
	87N	High-impedance restricted ground fault Intermittent ground fault		
	48/14	Starting time supervision, locked rotor		
	66/86	Restart inhibit		
	51M	Load jam protection, motor statistics		
	27/59	Undervoltage/overvoltage		
	81O/U	Underfrequency/overfrequency		
	27/Q	Undervoltage-controlled reactive power protection <sup>3)</sup>		
	27/47/59(N)	Flexible protection (index quantities derived from current and voltages): Voltage, power, p.f., rate-of-frequency-change protection		R H <sup>2)</sup>
■	Motor V, P, f Dir	67/67N Direction determination for overcurrent, phases and ground		
		48/14 Starting time supervision, locked rotor		
		66/86 Restart inhibit		
		51M Load jam protection, motor statistics		
		27/59 Under-/overvoltage		
		81O/U Under-/overfrequency		
		27/Q Undervoltage-controlled reactive power protection <sup>3)</sup>		
		27/47/59(N) Flexible protection (index quantities derived from current and voltages): Voltage, power, p.f., rate-of-frequency-change protection		H G
■	Motor	48/14 Starting time supervision, locked rotor		
		66/86 Restart inhibit		
		51M Load jam protection, motor statistics		H A
ARC, fault locator, synchro-check		Without		0
	79	With auto-reclosure		1
	21FL	With fault locator		2
	79, 21FL	With auto-reclosure, with fault locator		3
	25	With synchro-check <sup>3)</sup>		4
	25, 79, 21FL	With synchro-check <sup>3)</sup> , auto-reclosure, fault locator		7

■ Basic version included

V, P, f = Voltage, power, frequency protection

Dir = Directional overcurrent protection

IEF = Intermittent ground fault

1) 50N/51N only with insensitive ground-current transformer when position 7 = 1, 5, 7.

2) Sensitive ground-current transformer only when position 7 = 2, 6.

3) Synchro-check (no asynchronous switching), one function group; available only with devices 7SJ623, 7SJ624, 7SJ625 and 7SJ626.

4) with FW V4.90

# Overcurrent Protection/7SJ62

## Selection and ordering data

Description	Order No.	Order code
<b>7SJ62 multifunction protection relay</b>	<b>7SJ62</b> □□-□□□□□□-□□□□□□-□□□□	
<b>System interface (on rear of unit, Port B)</b>		
No system interface	0	
IEC 60870-5-103 protocol, RS232	1	
IEC 60870-5-103 protocol, RS485	2	
IEC 60870-5-103 protocol, 820 nm fiber, ST connector	3	
PROFIBUS DP Slave, RS485	9	L O A
PROFIBUS DP Slave, 820 nm wavelength, double ring, ST connector <sup>1)</sup>	9	L O B
MODBUS, RS485	9	L O D
MODBUS, 820 nm wavelength, ST connector <sup>2)</sup>	9	L O E
DNP 3.0, RS485	9	L O G
DNP 3.0, 820 nm wavelength, ST connector <sup>2)</sup>	9	L O H
IEC 60870-5-103 protocol, redundant, RS485, RJ45 connector <sup>2)</sup>	9	L O P
IEC 61850, 100 Mbit Ethernet, electrical, double, RJ45 connector (EN 100)	9	L O R
IEC 61850, 100 Mbit Ethernet, optical, double, LC connector (EN 100)2)	9	L O S
DNP3 TCP + IEC 61850, 100Mbit Eth, electrical, double, RJ45 connector <sup>3)</sup>	9	L 2 R
DNP3 TCP + IEC 61850, 100Mbit Eth, optical, double, LC connector <sup>3)</sup>	9	L 2 S
PROFINET + IEC 61850, 100Mbit Eth, electrical, double, RJ45 connector <sup>3)</sup>	9	L 3 R
PROFINET + IEC 61850, 100Mbit Eth, optical, double, LC connector <sup>3)</sup>	9	L 3 S

1) Not with position 9 = "B"; if 9 = "B", please order 7SJ6 unit with RS485 port and separate fiber-optic converters.

For single ring, please order converter 6GK1502-3AB10, not available with position 9 = "B".

For double ring, please order converter 6GK1502-4AB10, not available with position 9 = "B".

The converter requires a AC 24 V power supply (e.g. power supply 7XV5810-0BA00).

2) Not available with position 9 = "B".

3) available with V4.9

5

### Sample order

Position	Order No. + Order code
	7SJ622 5 - 5 E C 9 1 - 3 F A 1 + L O G
6 I/O's: 11 BI/6 BO, 1 live status contact	2
7 Current transformer: 5 A	5
8 Power supply: DC 110 to 250 V, AC 115 V to AC 230 V	5
9 Unit version: Flush-mounting housing, screw-type terminals	E
10 Region: US, English language (US); 60 Hz, ANSI	C
11 Communication: System interface: DNP 3.0, RS485	9
12 Communication: DIGSI 4, electric RS232	1
13 Measuring/fault recording: Extended measuring and fault records	3
14/15 Protection function package: Basic version plus directional TOC	F C
16 With auto-reclosure	1



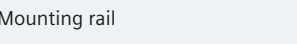
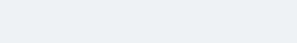


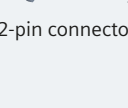
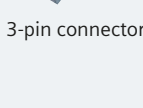


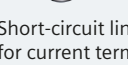
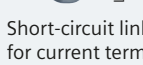
# Overcurrent Protection / 7SJ62

## Selection and ordering data

5

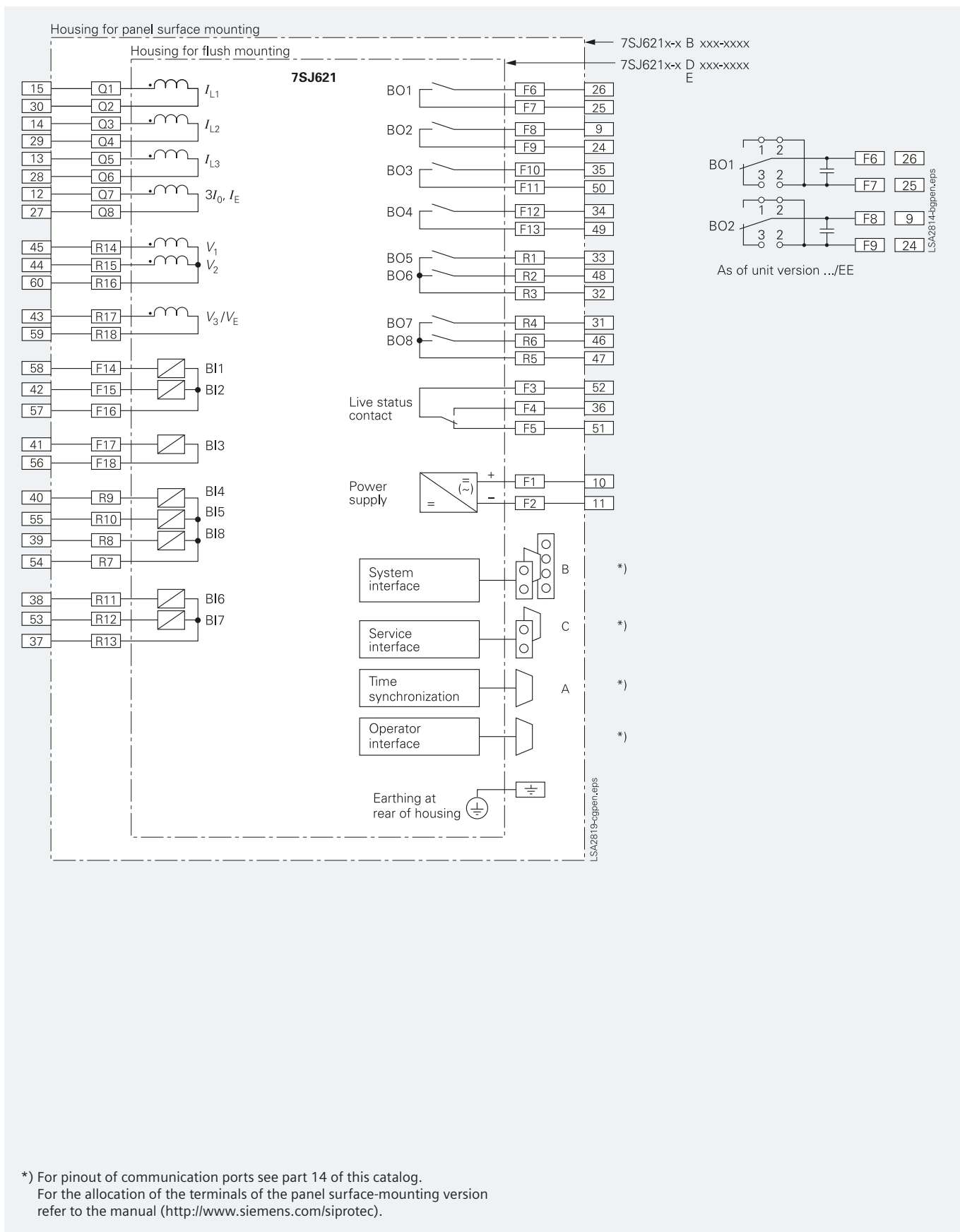
Accessories	Description	Order No.
	<b>Temperature monitoring box</b> AC/DC 24 to 60 V AC/DC 90 to 240 V	7XV5662-2AD10 7XV5662-5AD10
	<b>Varistor/Voltage Arrester</b> Voltage arrester for high-impedance REF protection 125 Vrms; 600 A; 1S/S 256 240 Vrms; 600 A; 1S/S 1088	C53207-A401-D76-1 C53207-A401-D77-1
	<b>Connecting cable</b> Cable between PC/notebook (9-pin con.) and protection unit (9-pin connector) (contained in DIGSI 4, but can be ordered additionally) Cable between temperature monitoring box and SIPROTEC 4 unit - length 5 m / 16.4 ft - length 25 m / 82 ft - length 50 m / 164 ft	7XV5100-4 7XV5103-7AA05 7XV5103-7AA25 7XV5103-7AA50
	<b>Manual for 7SJ62</b> English German	C53000-G1140-C207-x <sup>1)</sup> C53000-G1100-C207-6

1) x = please inquire for latest edition (exact Order No.).

Accessories	Description	Order No.	Size of package	Supplier
 LSP2289-afp.eps	Terminal safety cover			
	Voltage/current terminal 18-pole/12-pole	C73334-A1-C31-1	1	Siemens
	Voltage/current terminal 12-pole/8-pole	C73334-A1-C32-1	1	Siemens
	Connector 2-pin	C73334-A1-C35-1	1	Siemens
	Connector 3-pin	C73334-A1-C36-1	1	Siemens
	Crimp connector CI2 0.5 to 1 mm <sup>2</sup>	0-827039-1	4000 taped on reel	<sup>1)</sup>
	Crimp connector CI2 0.5 to 1 mm <sup>2</sup>	0-827396-1	1	<sup>1)</sup>
	Crimp connector: Type III+ 0.75 to 1.5 mm <sup>2</sup>	0-163084-2	1	<sup>1)</sup>
	Crimp connector: Type III+ 0.75 to 1.5 mm <sup>2</sup>	0-163083-7	4000 taped on reel	<sup>1)</sup>
	Crimping tool for Type III+ and matching female	0-539635-1 0-539668-2	1 1	<sup>1)</sup> <sup>1)</sup>
	Crimping tool for CI2 and matching female	0-734372-1 1-734387-1	1 1	<sup>1)</sup> <sup>1)</sup>
	Short-circuit links for current terminals	C73334-A1-C33-1	1	Siemens
	Short-circuit links for other terminals	C73334-A1-C34-1	1	Siemens
	Mounting rail for 19" rack	C73165-A63-D200-1	1	Siemens

1) Your local Siemens representative can inform you on local suppliers.





\*) For pinout of communication ports see part 14 of this catalog.  
 For the allocation of the terminals of the panel surface-mounting version refer to the manual (<http://www.siemens.com/siprotec>).

Fig. 5/46 7SJ621 connection diagram

# Overcurrent Protection / 7SJ62

## Connection diagram

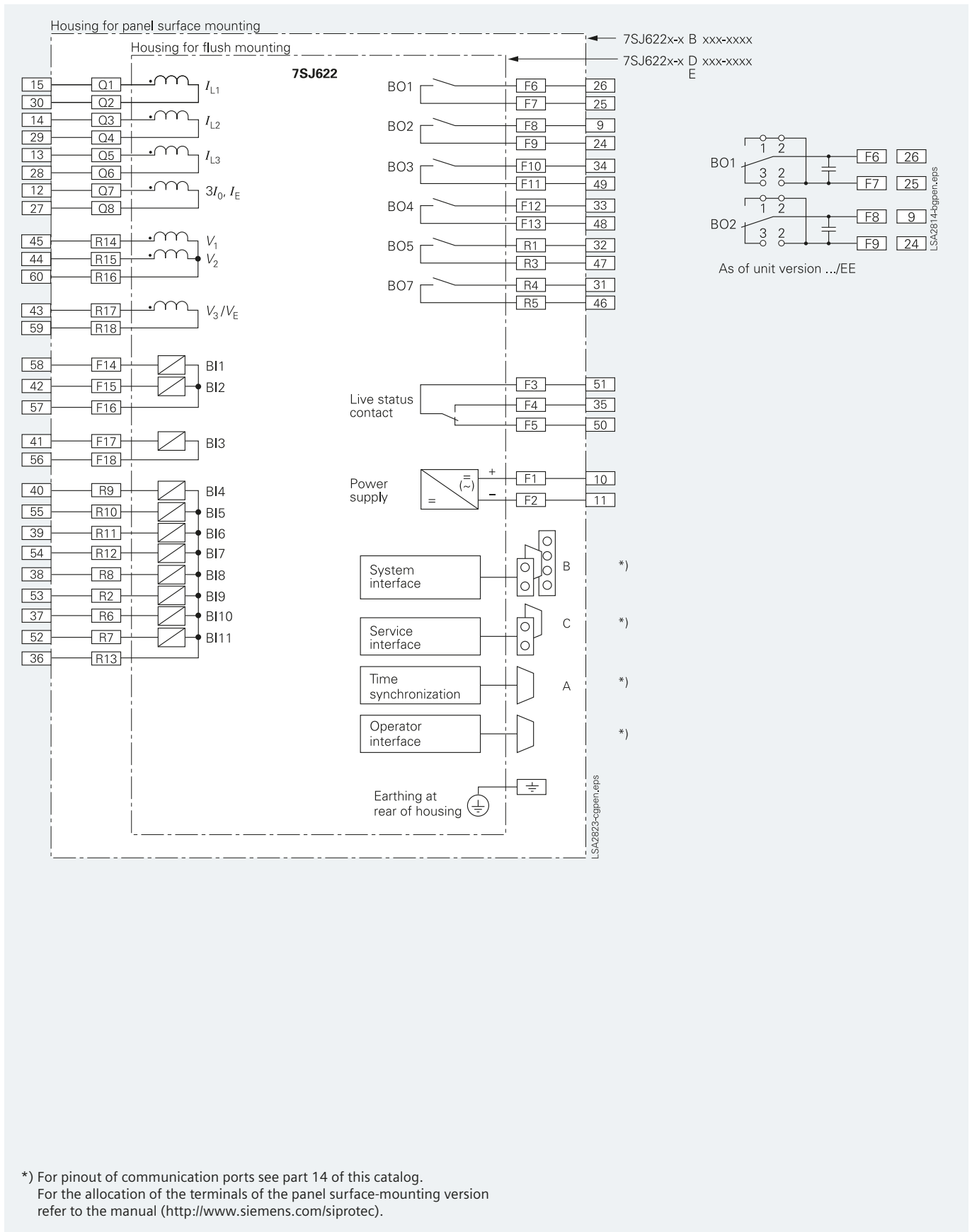
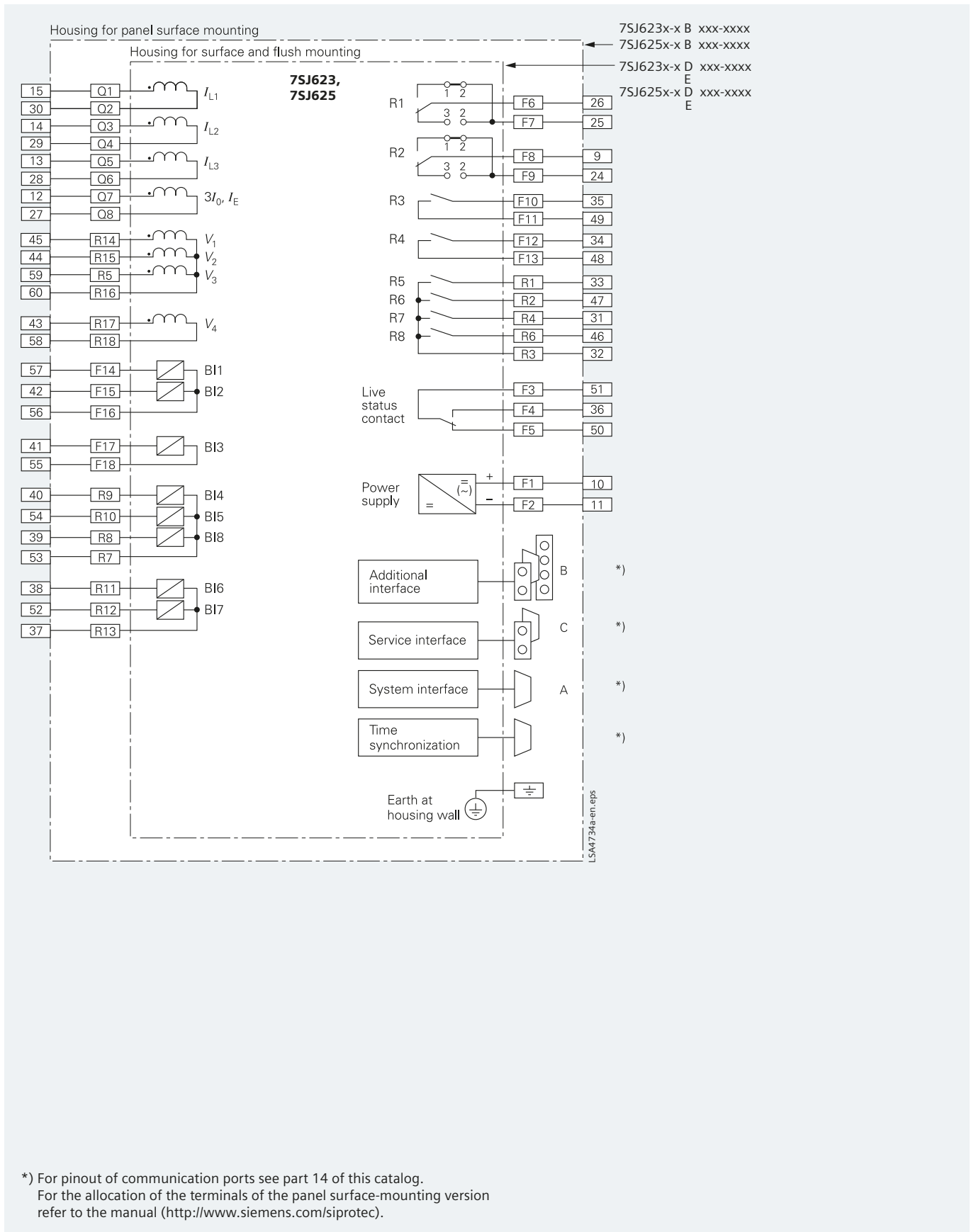


Fig. 5/47 7SJ622 connection diagram



\*) For pinout of communication ports see part 14 of this catalog.  
 For the allocation of the terminals of the panel surface-mounting version refer to the manual (<http://www.siemens.com/siprotec>).

Fig. 5/48 7SJ623, 7SJ625 connection diagram

# Overcurrent Protection / 7SJ62

## Connection diagram

5

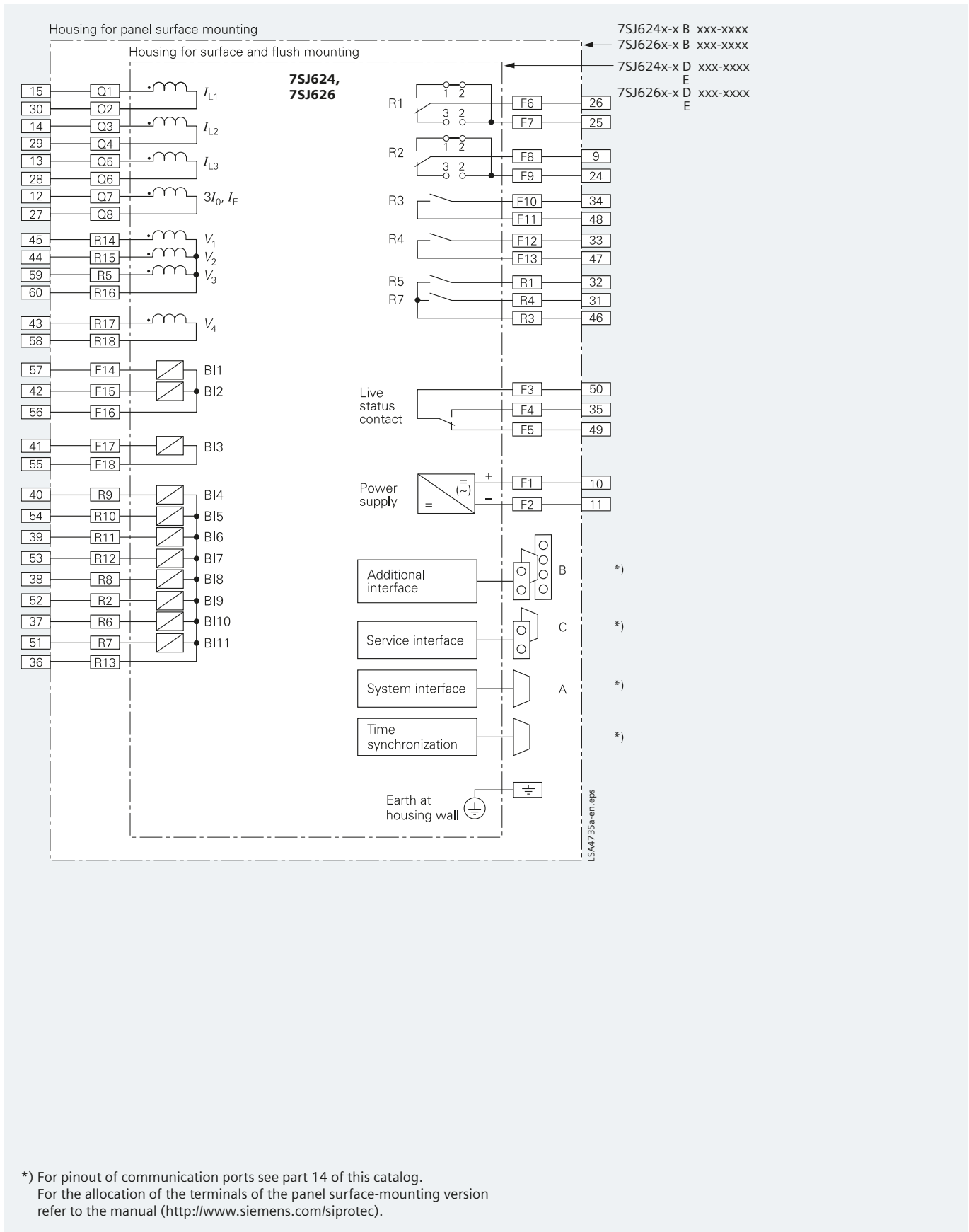


Fig. 5/49 7SJ624, 7SJ626 connection diagram